

SOURCE REGISTRATION AIR MANAGEMENT SERVICES

SEP 04 2015

Philadelphia Energy Solutions Refir ing and Marketing LLC 3144 Passyunk Avenue Philadelphia, PA 19145-5299 215-339-2000

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September 4, 2015

Mr. Edward Wiener Chief, Source Registration Air Management Services 321 University Avenue Philadelphia, PA 19104

Re: Philadelphia Energy Solutions Marketing and Refining LLC (PES)

Title V Permit No. V06-016

Revised Plan Approval Application: Tier 3 Project

Dear Mr. Wiener:

Enclosed are three copies of a revised Plan Approval Application plus an additional check for \$1,700 for the Tier 3 Project. The additional \$1,700 check is for the 870 H-3 Heater that is subject to NSPS Subpart Ja. This federally mandated project requires changes to several process units at the Philadelphia Energy Solutions (PES) Refir ing and Marketing LLC Philadelphia Refining Complex Point Breeze and Girard Point Refineries. These project changes will allow additional sulfur treatment of gasoline components so that the refinery's gasoline product will meet USEPA's Tier 3 requirements by the January 1, 2017 deadline.

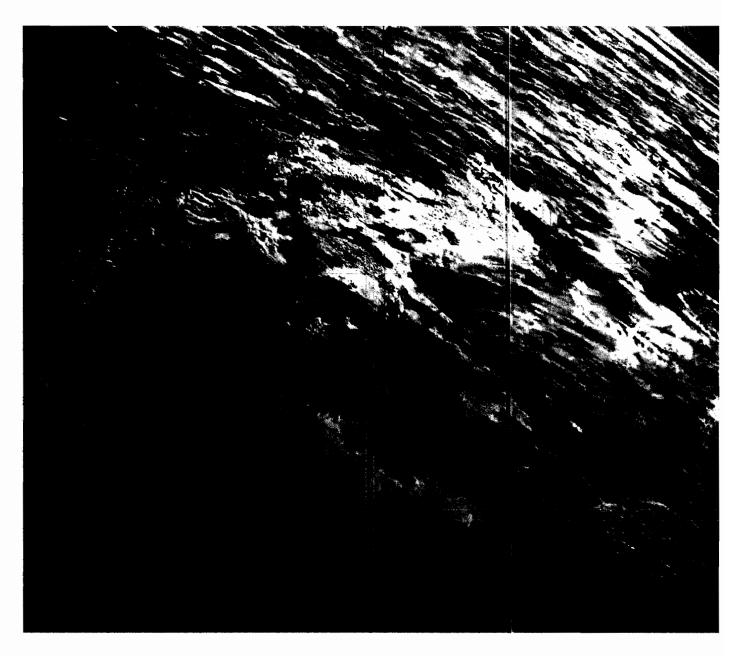
Please review this application and let me know if you have any questions or would like to meet. Please contact me at 215-339-2074.

Respectfully,

Charles D. Barksdale, Jr.

Site Environmental Director

CBD/dc





Philadelphia Energy Solutions Refining and Marketing LLC

Tier 3 Project Philadelphia, Pennsylvania

September 2015

Environmental Resources Management 75 Valley Stream Parkway, Suite 200 Malvern, PA 19355 (484) 913-0300

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		ERM i	PES TIER 3 PROJECT
	4.1	GREENHOUSE GAS TAILORING RULE .	17
4.0	NEV	V SOURCE REVIEW APPLICABILITY	17
	3.6	TOTAL PROJECT EMISSIONS	15
	3.5	FUGITIVE EMISSIONS - PIPING COMPONENTS	15
		3.4.1 Incremental Cooling Water Emissions3.4.2 Incremental Sulfur Production Emissions	13 14
	3.4	ANCILLARY SOURCES AND UTILITIES EMISSIONS	13
	3.3	UNIT 1332 HYDROBON STRIPPER AND PRE-FRACTIONATOL EMISSIONS	R 12
	3.2	UNIT 870 LSG UNIT EMISSIONS	11
	3.1	UNIT 864 NAPHTHA HYDROTREATING UNIT EMISSIONS	9
3.0	DET	AILED PROJECT EMISSIONS ANALYSIS	8
	2.6	PROJECT SCHEDULE	6
	2.5	NEW FUGITIVE EMISSIONS COMPONENTS	6
	2.4	ANCILLARY SOURCES AND UTILITIES	6
	2.3	UNIT 1332 HYDROBON STRIPPER AND PRE-FRACTIONATOR	R 5
	2.2	UNIT 870 LSG UNIT	4
	2.1	UNIT 864 NAPHTHA HYDROTREATING UNIT	4
2.0	PRO	OJECT OVERVIEW	4
	1.3	PLAN APPROVAL APPLICATION CONTENT	3
	1.2	PES TIER 3 PROJECT	2
	1.1	TIER 3 GASOLINE	1
1.0	INT	RODUCTION	1
TAB	LE OF	CONTENTS	

	4.2	PREVENTION OF SIGNIFICANT DETERIORATION ANALYSIS	18
	4.3	NONATTAINMENT NEW SOURCE REVIEW ANALYSIS - OZONE	19
5. 0	BAT	DETERMINATION	22
	5.1	NO _X CONTROLS	23
	5.2	CO CONTROLS	24
	5.3	PM/PM ₁₀ /PM _{2.5} CONTROLS	25
	5.4	SO ₂ CONTROLS	25
	5.5	VOC CONTROLS	26
6.0	APP	LICABLE STANDARDS ANALYSIS	28
	6.1	AIR MANAGEMENT SERVICES REGULATIONS	28
	6.2	FEDERAL NESHAPS (40 CFR PART 63)	28
	6.3	FEDERAL NSPS (40 CFR PART 60) 6.3.1 Replacement Unit 864 PH-7R Heater 6.3.2 Unit 870 H-2 Heater 6.3.3 New Unit 870 H-3 Heater 6.3.4 Other Affected Heaters	29 29 29 30 30
LIST	OF TA	BLES	
	1-1	USEPA Estimates of Nationwide Emissions Reductions from the Tier 3 Stand	dards
	2-1	Fugitive Equipment Components	
	3-1	Expected and Potential Firing Rates of Each Affected Henrer	
	3-2	Projected Unit 864 Naphtha Hydrotreating Unit Heater Emissions	
	3-3	Unit 864 PH-7 Heater Shutdown Emissions	
	3-4	Projected Unit 870 LSG Unit Heater Emissions	
	3-5	Projected Unit 1332 Hydrobon Stripper and Pre-Fractionator Incremental	

- 3-6 Projected Incremental Cooling Water Emissions
- 3-7 Projected Incremental Sulfur Production Emissions
- 3-8 Projected Fugitive Component Emissions
- 3-9 Total PES Tier 3 Project Emissions
- 4-1 PSD Emissions Analysis (Step 1)
- 4-2 NANSR Netting Analysis for NO_x and VOC Emissions (5 calendar year)
- 4-3 NANSR Netting Analysis for NO_x and VOC Emissions (10 year)
- 5-1 Affected Heater Construction Dates

LIST OF ATTACHMENTS

- A AMS Plan Approval Application Forms
- B Site Location Map/Process Flow Diagrams
- C Back-up Emissions Calculations
- D Contemporaneous Emissions Tables
- E Best Available Technology NO_x Control Cost Effectiveness Calculations

1.0 INTRODUCTION

Philadelphia Energy Solutions Refining and Marketing, LLC (PES) owns and operates the Philadelphia Refining Complex (Complex) – including the Point Breeze Refinery, Girard Point Refinery, and the Schuylkill River Tank Farm. At the Philadelphia Refining Complex, PES is currently permitted to operate numerous desulfurization and hydrotreating processes at the Refinery under an existing permit (Title V Operating Permit No. V06-016). PES plans to reconfigure existing process units, re-route intermediate process streams, and expand hydrotreating process capacity to enable compliance with the Tier 3 gasoline standards. For the purpose of this application, the project is referred to as the "PES Tier 3 Project" or "Project."

1.1 TIER 3 GASOLINE

The United State Environmental Protection Agency (USEPA) promulgated new standards for the sulfur content in gasoline in April 2014 referred to as the Tier 3 standards. Under the Tier 3 standards, gasoline will be required to meet an annual average standard of 10 parts per million by weight (ppmw) of sulfur by January 1, 2017. These standards are an extension of the Tier 2 standards, promulgated in February 2000, which required gasoline to meet an annual average standard of 30 ppmw.

USEPA estimates that the following nationwide reductions from onroad vehicles in **Table 1-1** below in nitrogen oxides (NC₂), volatile organic compounds (VOC), carbon monoxide (CO), direct particulate matter less than 2.5 microns (PM_{2.5}), and sulfur dioxide (SO₂) in 2018 and 2030.

Table 1-1 USEPA Estimates of Nationwide Emissions Reductions from the Tier 3
Standards

	2018			2030	
Pollutant	Tons	% of Onroad inventory	Tons	% of Onroad inventory	
NO _x	264,369	10	328,509	25	
VOC	47,504	3	167,591	16	
СО	278,879	2	3,458,041	24	
PM _{2.5}	130	0.1	7,892	10	
SO ₂	14,813	56	12,399	56	

1.2 PES TIER 3 PROJECT

PES is proposing to make several operational and process changes to comply with the Tier 3 standards. The PES Tier 3 Project includes expansion of the sulfur removal capacity of the Unit 864 Naphtha Hydrotreating Unit and the Unit 870 Low Sulfur Gasoline (LSG) Unit at the Point Breeze Refinery as well as piping changes at the front end of the Unit 1332 Reformer Unit at the Girard Point Refinery. The changes will allow additional sulfur treatment, but not additional production, of finished gasoline, straight run naphtha, and other gasoline blending streams currently generated and processed at the refinery.

Proposed changes associated with the PES Tier 3 Project including the following:

- Expand the capacity of the Unit 864 Naphtha Hydrotreating Unit from 40 thousand barrels per day (MBPD) to a nominal 48 MBPD;
- Expand the capacity of the Unit 870 LSG Unit from 65 MBPD to a nominal 84 MBPD;
- Utilize the existing Unit 1332 hydrobon reactor to produce sweet naphtha for gasoline blending;
- Utilize vacuum deaerated water in the existing Unit 433 Alkylate Water Wash Tower¹ to remove water soluble sulfolane from alkylate products;
- Installation of low NO_x burners (LNB) on the Unit 864 PH-1, Unit 864 PH-11, Unit 864 PH-12 refinery fuel gas fired heaters;
- Replacement of the Unit 864 PH-7 Heater with an idle heater from the former Sunoco Inc. (R&M) Eagle Point Refinery; and
- Installation of a new Unit 870 H-3 Heater.

The proposed installations are fully described in this permit application submitted to Air Management Services (AMS) by PES. PES has evaluated the emission changes associated with this Project and determined that the provisions of the Prevention of Significant Deterioration (PSD) do not apply;

•

Note the use of vacuum deaerated water in the Unit 433 Alkylate Water Wash Tower process does not introduce air pollutant emissions to the atmosphere; therefore, it will not be discussed further in this plan approval application.

however, nonattainment New Source Review (NANSR) regulations are triggered by this Project.

1.3 PLAN APPROVAL APPLICATION CONTENT

This plan approval describes the proposed new sources and regulatory analysis related to the PES Tier 3 Project. A more detailed description of the Project and the emissions associated with the Project are provided in Sections 2 and 3, respectively. A summary of the results of PSD and NANSR applicability analysis are presented in Section 4. The Best Available Technology Review is provided in Section 5. Reviews of applicable local, State and federal regulatory requirements are presented in Sections 6. Additional Project-related information is provided in the attachments as follows:

- AMS Plan Approval Application Forms (Attachment A);
- Site Location Map/Process Flow Diagrams (Attachment B);
- Back-up Emission Calculations (Attachment C);
- Contemporaneous Emissions Tables (Attachment D); and
- Best Available Technology NO_x Control Cost Effectiveness Calculations (Attachment E).

2.0 PROJECT OVERVIEW

In this Project, PES is proposing to make operational and process changes to further desulfurize existing gasoline, straight run naphtha and other gasoline blending streams to meet the Tier 3 standards in the future. The expansions of the Unit 864 Naphtha Hydrotreating Unit and Unit 870 LSG Unit as well as the piping changes to the Unit 1332 hydrobon stripper and pre-fractionator are discussed in the sections below.

2.1 UNIT 864 NAPHTHA HYDROTREATING UNIT

In this Project, PES plans to expand the capacity of the Unit 864 Naphtha Hydrotreating Unit from 40 MBPD to a nominal 48 MBPD by re-traying towers; re-piping and re-routing streams within the unit; replacing or modifying charge, bottoms, and reflux pumps; and modifying and replacing fired heaters. An overall process flow diagram of the proposed changes to the Unit 864 Naphtha Hydrotreating Unit is included in **Attachment B**.

As a result of this Project, all fired heaters (Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12) associated with the Unit 864 Naphtha Hydrotreating Unit are expected to have increased utilization. Furthermore, PES will be replacing the existing Unit 864 PH-7 Heater (nominal firing duty of 45.0 million British Thermal units per hour [MMBtu/hr]) with an existing idle heater (LSG H-1) located at the former Sunoco Inc. (R&M) Eagle Point Refinery in New Jersey². The replacement Unit 864 PH-7R Heater will include ultra-low NO_x burners (ULNB) for NO_x control and will have nominal firing duty of 70.0 MMBtu/hr.

As part of the Project, PES also plans to install LNB on the existing Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12 Heaters.

2.2 UNIT 870 LSG UNIT

The Unit 870 LSG Unit currently operates two parallel desulfurization trains with two reactors in series in each train to remove sulfur from fuels. In this Project, PES plans to expand the capacity from 65 MBPD to 84 MBPD by installing a new splitter tower between the reactors where splitter tower light ends will go to gasoline blending while the splitter tower bottoms will

² Sunoco Inc. (R&M) Eagle Point Facility (55781) Emission Unit U45.

be further desulfurized by the remainder of Unit 870 LSG Unit. The new splitter tower reboiler will require the installation of a new refinery fuel gas fired heater, Unit 870 H-3 Heater, with a nominal firing duty of 110.0 MMBtu/hr equipped with ULNB for NO_x control. Other changes include adding pumps; re-routing piping; and installing new heat exchangers within the unit to allow for the expanded capacity. An overall process flow diagram of the proposed changes to the Unit 870 LSG Unit is included in **Attachment B**.

Also, as a result of this Project, both fired heaters (Unit 870 H-1 and Unit 870 H-2) associated with the Unit 870 LSG Unit are expected to have increased utilization, which will remain within each heater's existing firing rate limit. Both heaters currently have ULNB installed for NO₃ control. However, it was determined during the design phases for the Unit 870 LSG Unit that the existing ULNBs installed in the Unit 870 H-2 Heater will be replaced with a newer version of the same ULNB. Both the maximum firing capacity (MMBtu/hr) and NO₃ emission rate (lb/MMBtu) of the Unit 870 H-2 Heater will be unaffected by the change.

2.3 UNIT 1332 HYDROBON STRIPPER AND PRE-FRACTIONATOR

The 1332 Reformer Unit includes the pre-fractionator, hydrobon reactor system, hydrobon stripper system, and reformer/platformer. PES has determined that piping changes around the Unit 1352 hydrobon reactor system can be made to allow the unit to produce sweet naphtha for gasoline blending. To accomplish this, PES plans to re-route a portion of the hydrobon stripper bottoms to sweet naphtha storage tanks and re-route the pre-fractionator overhead to the Unit 864 Naphtha Elydrotreating Unit for further processing. An overall process flow diagram of the proposed changes to the Unit 1332 hydrobon stripper and pre-fractionator is included in Attachment B.

The changes listed above will not increase the overall capacity of the Unit 1332 Reformer Unit; however, both the Unit 1332 H-2 (ULNB currently installed) and Unit 1332 H-3 Heaters are expected to have increased utilization as a result of the Project. Furthermore, the type of material stored and the overall throughput of the sweet naphtha storage tanks will not be affected by this Project.

2.4 ANCILLARY SOURCES AND UTILITIES

The PES Tier 3 Project will expand the gasoline hydrotreating capacity of the Complex thus expanding the incremental utilization of ancillary utilities such as steam generating sources, cooling towers, and the Unit 867 Sulfur Recovery Unit (SRU) relative to their baseline period. The following approximate impacts from ancillary sources and utilities are expected as a result of the Project:

- 600 gallons per minute (gpm) of incremental cooling water will be required at the Unit 864 Naphtha Hydrotreating Unit, which will be processed by the existing Unit 864 Cooling Tower; and
- 0.45 tons per day (TPD) of incremental sulfur production as a result of additional sulfur being removed from finished gasoline, straight run naphtha, and other gasoline blending streams.

2.5 NEW FUGITIVE EMISSIONS COMPONENTS

Additional fugitive emissions components including valves, pressure relief devices, and flanges/connectors associated with the proposed changes will be installed as a part of this Project. A conservatively estimated list of fugitive components planned for this Project is summarized in **Table 2-1** below.

Table 2-1 Fugitive Equipment Components

Equipment	Number of Components
Valves	125
Flanges	250
Connectors	-
Pump Seals	13
Other	-

2.6 PROJECT SCHEDULE

PES is planning to make the proposed changes to refinery units during scheduled turnarounds starting in the fourth quarter 2015. As noted above,

construction must begin as soon as possible to ensure the Complex is producing Tier 3 gasoline by January 1, 2017.

This section describes the calculations and assumptions made to estimate the emissions associated with PES Tier 3 Project. The emissions from the proposed Project including nitrogen oxides (NO_x), nitrogen dioxide (NO_2), sulfur dioxide (SO_2), carbon monoxide (CO), volatile organic compounds (VOC), particulate matter (PM), particulate matter less than 10 microns (PM_{10}), particulate matter less than 2.5 microns ($PM_{2.5}$), lead, and greenhouse gas (PM_2) emissions (shown as carbon dioxide equivalents [PM_2] are detailed below. **Table 3-9** at the end of this section shows the total PES Tier 3 Project emissions. Detailed emissions calculations are presented in **Attachment C**.

PES has determined that certain emissions sources associated with the Unit 864 Naphtha Hydrotreating Unit and Unit 870 LSG Unit have been "modified" due a physical change or a change in the method of operation of the source. In the case of this Project, due to the expansion of treating capacity of both units, the following fired heaters will have a change in the method of operation as defined in 25 PA Code §121.1:

- Unit 864 PH-1 Heater;
- Unit 864 PH-11 Heater;
- Unit 864 PH-12 Heater;
- Unit 870 H-1 Heater; and
- Unit 870 H-2 Heater.

The emissions changes from the modified heaters are calculated as the difference between the baseline actual emissions (BAE) and the future projected actual emissions (PAE). As per 25 PA Code §127.203a(a)(4)(i) and 40 Code of Federal Regulations (CFR) §52.21(b)(48), BAE were estimated as the highest annual average "during a consecutive 24-month period selected by the owner or the operator within the 5-year period immediately prior to the date a complete plan approval application is received by the Department." Furthermore, the PAE for each modified fired heater are based on the existing hourly firing limits found in Title V Operating Permit No. V06-016 and the RACT Plan Approval issued February 19, 2014.

Note that the Unit 864 PH-7 Heater will be replaced with a heater from the former Sunoco Inc. (R&M) Eagle Point Refinery, which will be considered a

new emissions source for PSD and NANSR purposes. The new splitter tower reboiler at the Unit 870 LSG Unit will require the installation of the new Unit 870 H-3 Heater. The Unit 864 PH-1 Heater has demonstrated an inability to operate at its current potential firing rate of 80.0 MMBtu/hr; therefore, the potential firing rate will be reduced to 74.9 MMBtu/hr. Lastly, the Unit 1332 H-2 and Unit 1332 H-3 Heaters are only expected to experience an increase in utilization as a result of this Project and are not being physically modified or debottlenecked.

The annual average expected firing rates and potential firing rates of each fired heater affected by the PES Tier 3 Project are shown in **Table 3-1** below.

Table 3-1 Expected and Potential Firing Rates of Each Affected Heater

Fired Heater	Annual Average Expected Firing Rate (MMBtu/hr)	otential Firing Rate (MMBtu/hr)1
Unit 864 PH-1	47.8	74.9
Unit 864 PH-72	56.3	70.0
Unit 864 PH-11	58.9	74.0
Unit 864 PH-12	63.0	85.1
Unit 870 H-1	91.2	97.0
Unit 870 H-2	49.9	53.0
Unit 870 H-33	103.7	110.0
Unit 1332 H-2	43.8	60.0
Unit 1332 H-3	28.1	43.0

With the exception of the Unit 864 PH-1, Unit 864 PH-7R, and Unit 370 H-3 Heaters, the potential firing rates match the existing hourly firing rate limits found in Title V Operating Permit No. V06-016 and the RACT Plan Approval issued February 19, 2014.

3.1 UNIT 864 NAPHTHA HYDROTREATING UNIT EN'ISSIONS

The reconfiguration of the Unit 864 Naphtha Hydrotreating Unit will increase emissions from the Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12 Heaters. The BAE are based on the actual firing from each of these heaters during the period of June 2012 through May 2014. The annual emission changes in this Project reflect the difference between past actual emissions (BAE) and future projected actual emissions (PAE) based on the existing hourly firing rate limits.

This heater will be replaced with the existing LSG H-1 Heater from the former Sunoco Inc. (R&M) Eagle Point Refinery.

³ This will be a new heater installed to provide the necessary heat for the new splitter tower reboiler.

This Project will result in an increase in firing of certain heaters; however, it is not expected to have an impact on the amount of sulfur in the refinery fuel gas, which is the only fuel for refinery heaters. Therefore, SO₂ emissions are calculated using heater-specific SO₂ emission factors based on average actual firing rates and average actual SO₂ emissions from 2013 and 2014. Consistent with historic practices, PES used USEPA AP-42 emission factors for VOC, PM, PM₁₀, PM_{2.5}, and CO. The CO₂e emissions were calculated using emission factors from the Greenhouse Gas Mandatory Reporting Rule (GHGMRR) codified at 40 CFR Part 98.

The Unit 864 PH-7 Heater is being replaced with an idle heater (LSG H-1) located at the Eagle Point Refinery; therefore, there are no past actual emissions associated with this source and PAE will be based on the source's potential to emit (PTE). This replacement heater, Unit 864-PH-7R, is equipped with ULNB that will achieve a NO_x emission rate of 0.02 pounds per MMBtu (lb/MMBtu). Also as part of the Project, PES has elected to install LNB on the Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12 Heaters that will achieve a NO_x emission rate of 0.06 lb/MMBtu.

The annual emissions in tons per year (TPY) for each Unit 864 Naphtha Hydrotreating Unit heaters are shown below in **Table 3-2**.

Table 3-2 Projected Unit 864 Naphtha Hydrotreating Unit Heater Emissions

Pollutant	Unit 864 PH-1 Heater (TPY)	Unit 864 PH-7R Heater (TPY)	Unit 864 PH-11 Heater (TPY)	Unit 864 PH-12 Heater (TPY)	Total Unit 864 Emissions (TPY)
NO _x 1	-2.6	6.5	-6.2	-4.4	-6.8
NO ₂		6.5			6.5
SO ₂	0.5	0.9	0.4	0.4	2.2
СО	15.9	9.7	12.0	12.1	49.7
PM	1.4	2.3	1.1	1.1	5.9
PM ₁₀	1.4	2.3	1.1	1.1	5.9
PM _{2.5} ²	1.4	0.7	1.1	1.1	4.3
VOC	1.0	1.6	0.8	0.8	4.2
Lead	9.4E-05	1.5E-04	7.1E-05	7.2E-05	3.9E-04
CO₂e	22,758	35,902	17,213	17,341	93,214

¹ NO_x emissions for the Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12 heaters are based on the sum of the Project emissions for this source (PAE minus BAE) under 25 PA §127.203(b)(1)(i). Under 25 PA Code §127.203a(a)(1)(ii), NO₂ emissions for these heaters are based on Step 1 emissions increases only, where these sources are not expected to have an increase in NO₂ emissions.

² The Unit 864 PH-7R Heater, originally installed at the LSG Unit at the former Eagle Point Refinery, has an identical design as the Unit 870 H-1 and Unit 870 H-2 Heaters. Therefore, the PM_{2.5} emissions rate as demonstrated by stack testing at the Unit 870 LSG Unit heaters was used for the Unit 864 PH-7R Heater.

The emissions associated with the shutdown of the existing Unit 864 PH-7 Heater are the annual average emissions based actual emissions for the period of June 2012 through May 2014. The shutdown emissions decreases for the Unit 864 PH-7 Heater are shown in **Table 3**·3 below.

Table 3-3 Unit 864 PH-7 Heater Shutdown Emissions

Pollutant	Total Unit 864 PH-7 Heater Shutdown Emissions (TPY)
NO_x	-10.2
SO ₂	-0.3
СО	-9.9
PM	-0.9
PM ₁₀	-0.9
PM _{2.5}	-0.9
VOC	-0.7
Lead	-5.9E-05
CO₂e	-13,511

3.2 UNIT 870 LSG UNIT EMISSIONS

The expansion of the Unit 870 LSG Unit will increase emissions from the Unit 870 H-1 Heater and the Unit 870 H-2 Heater. The BAE for the Unit 870 H-1 and Unit 870 H-2 Heaters are based on the actual firing from each of these heaters during the period of June 2012 through May 2014. The annual emission changes in this Project reflect the difference between past actual emissions (BAE) and future projected actual emissions (PAE) based on the existing hourly firing rate limits.

NO_x, PM, PM₁₀, PM_{2.5}, VOC, and CO emission factors were developed for the Unit 870 H-1 and Unit 870 H-2 Heaters based on stack testing. Similar to the Unit 864 Naphtha Hydrotreating Unit heaters, SO₂ emissions are calculated using heater-specific SO₂ emission factors based on average actual firing rates and average actual SO₂ emissions from 2013 and 2014. The CO₂e emissions were calculated using emission factors from the GHGMRR codified at 40 CFR Part 98. As part of the installation of the new splitter tower in the Unit 870 LSG Unit, the new Unit 870 H-3 Heater will be

installed to provide the necessary heat for the splitter tower reboiler. This heater will be equipped with ULNB that will achieve a NO_x emission rate of 0.03 lb/MMBtu.

The annual emissions for each of the Unit 870 LSG Unit heaters are shown below in **Table 3-4**.

Table 3-4 Projected Unit 870 LSG Unit Heater Emissions

Pollutant	Unit 870 H-1 Heater (TPY)	Unit 870 H-2 Heater (TPY)	Unit 870 H-3 Heater (TPY)	Total Unit 870 Emissions (TPY)
NO _x	7.8	2.6	14.5	24.9
NO ₂	7.8	2.6	14.5	24.9
SO ₂	0.6	0.3	1.1	2.0
СО	0.4	0.0	14.5	14.8
PM	1.7	0.2	3.6	5.5
PM ₁₀	1.7	0.2	3.6	5.5
PM _{2.5}	0.6	0.2	1.1	1.9
VOC	0.1	0.1	2.4	2.6
Lead	1.3E-04	4.5E-05	2.3E-04	4.1E-04
CO ₂ e	31,413	10,943	56,417	98,773

3.3 UNIT 1332 HYDROBON STRIPPER AND PRE-FRACTIONATOR EMISSIONS

The fugitive VOC emissions from piping connections planned for the Unit 1332 hydrobon stripper and pre-fractionator are included in **Section 3.5** below.

The BAE are based on the actual firing from the Unit 1332 H-2 and Unit 1332 H-3 Heaters during the period of June 2012 through May 2014. The annual emission changes in this Project reflect the difference between past actual emissions (BAE) and future projected actual emissions (PAE) based on the expected average hourly firing rate of these heaters as a result of this Project. That is, the emissions increases are based on the incremental demand on these non-modified heaters due to increased processing of streams through the hydrobon equipment.

NO_x and CO emission factors were developed for the Unit 1332 H-2 Heater based on stack testing, while USEPA AP-42 emissions factors were used for

NO_x and CO emissions from the Unit 1332 H-3 Heater. Consistent with historic practices for both heaters, PES used USEPA AP-42 emission factors for VOC, PM, PM₁₀, and PM_{2.5}. Similar to the Unit 864 Naphtha Hydrotreating Unit heaters, SO₂ emissions are calculated using heater-specific SO₂ emission factors based on average actual firing rates and average actual SO₂ emissions from 2013 and 2014. The CO₂e emissions were calculated using emission factors from the GHGMI'R codified at 40 CFR Part 98. The annual emissions for the Unit 1332 hydrobon stripper and pre-fractionator are shown below in **Table 3-5**.

Table 3-5 Projected Unit 1332 Hydrobon Stripper and Pre-Fractionator Incremental Emissions

Pollutant	Unit 1332 H-2 Heater (TPY)	Unit 1332 H-3 Heater (TPY)	Total Unit 1332 I missions (TPY)
NO _x	1.6	1.6	3.2
NO ₂	1.6	1.6	3.2
SO ₂	0.2	0.1	0.2
СО	0.5	1.4	1.9
PM	0.4	0.1	0.5
PM ₁₀	0.4	0.1	0.5
PM _{2.5}	0.4	0.1	0.5
VOC	0.3	0.1	0.4
Lead	2.4E-05	8.1E-06	3.2E-05
CO ₂ e	6,079	2,018	8,097

3.4 ANCILLARY SOURCES AND UTILITIES EMISSIONS

The PES Tier 3 Project will result in incremental demand on ancillary utilities such as cooling towers and the Unit 867 Sulfur Receivery Unit (SRU) relative to their baseline period. The sections below describe the emissions and calculations for each source.

3.4.1 Incremental Cooling Water Emissions

The incremental 600 gpm of incremental cooling water will be processed by the existing Unit 864 Cooling Tower. The emissions calculations assume an incremental recirculation rate of 600 gpm, an expected maximum dissolved solids concentration of 600 ppmw, and drift eliminator performance of 0.005%. USEPA's AP-42 Chapter 5 emission factors are used to provide a

conservative estimate for potential VOC emissions. Emissions for PM, PM₁₀, and PM_{2.5} are estimated based on the Reisman/Frisbie methodology³. The annual emissions for incremental cooling water are shown in **Table 3-6** below.

Table 3-6 Projected Incremental Cooling Water Emissions

Pollutant	Incremental Cooling Water Emissions (TPY)
PM	0.2
PM ₁₀	0.1
PM _{2.5}	0.001
VOC	0.1

3.4.2 Incremental Sulfur Production Emissions

Based on an engineering analysis of the total sulfur reduction expected in the gasoline blending pool as a result of this Project, an incremental 0.45 TPD of sulfur production will be expected at the Unit 867 SRU. Emissions for NO_x , SO_2 , and CO were developing by scaling actual Unit 867 SRU emissions and sulfur production for 2013 with the expected incremental sulfur production as a result of this Project. The annual emissions for incremental sulfur production are shown in **Table 3-7** below.

Table 3-7 Projected Incremental Sulfur Production Emissions

Pollutant	Incremental Sulfur Production Emissions (TPY)
NOx	0.1
NO ₂	0.1
SO ₂	0.2
СО	3.3

³ Reisman, J. and Frisbie, G., Calculating Realistic PM10 Emissions From Cooling Towers.

3.5 FUGITIVE EMISSIONS - PIPING COMPONENTS

This proposed Project will result in an increase in VOC emissions from equipment leaks due to the installation of equipment such as flanges and valves required as part of the piping installations. PES has conservatively estimated a component count, including valves, flanges, connectors and pumps based on preliminary engineering design. Consistent with current PES practices, the emission increases from equipment leaks were calculated based on USEPA emission factors for the petroleum industry. Fugitive VOC emissions in tons per year from leaking equipment for the proposed Project are presented in **Table 3-8** below.

Table 3-8 Projected Fugitive Component Emissions

Affected Units	New Fugitive Components	Number of Components	VOC Emissions (TPY) ¹
	Valves	125	0.009
Unit 864, Unit 870, and Unit 1332	Flanges	250	0.001
OHH 1552	Pumps	13	0.003
T	0.013		

¹ Consistent with current PES practice, potential fugitive emissions are estimated based on the USEPA "Protocol for Equipment Leak Emission Estimates", EPA-453/R-95-017, Table 2-12.

3.6 TOTAL PROJECT EMISSIONS

The total emissions from the PES Tier 3 Project are summarized in **Table 3-9** below.

3					Pc	Pollutant (TPY)	(YY)				
Source	NOx	NO2	SO_2	00	VOC	PM	PM_{10}	PM _{2.5}	H ₂ SO ₄	Lead	COze
Unit 864 PH-1 Heater	-2.6		0.5	15.9	1.0	1.4	1.4	1.4	:	9.4E-05	22,758
Unit 864 PH-7 Heater1	-10.2				-0.7	:	:	:	;	:	:
Unit 864 PH-7R Heater	6.5	6.5	6.0	6.7	1.6	2.3	2.3	0.7	:	1.5E-04	35,902
Unit 864 PH-11 Heater	-6.2		6.4	12.0	8.0	1.1	1.1	1.1	:	7.1E-05	17,213
Unit 864 PH-12 Heater	4.4		9.4	12.1	8.0	1.1	1.1	1.1	;	7.2E-05	17,341
Unit 870 H-1 Heater	7.8	7.8	9.0	0.4	0.1	1.7	1.7	9.0	:	1.3E-04	31,413
Unit 870 H-2 Heater	2.6	2.6	0.3	0.0	0.1	0.2	0.2	0.2	:	4.5E-05	10,943
Unit 870 H-3 Heater	14.5	14.5	1.1	14.5	2.4	3.6	3.6	1.1	:	2.3E-04	56,417
Unit 1332 H-2 Heater	1.6	1.6	0.2	0.5	0.3	0.4	0.4	0.4	:	2.4E-05	6/0/9
Unit 1332 H-3 Heater	1.6	1.6	0.1	1.4	0.1	0.1	0.1	0.1	:	8.1E-06	2,018
Incremental Cooling Water					0.1	0.2	0.1	0.001			
Incremental Sulfur Production	0.1	0.1	0.2	3.3							
Fugitive Components					0.01						
Total Project Emissions	11.2	34.6	4.7	69.7	6.7	12.0	12.0	6.7	0	8.3E-04	200,084
											ļ

¹ Consistent with 25 PA Code §127.203(b)(1)(i), the proposed increases or decreases in emissions from the project are aggregated. Therefore, the Unit 864 PH-7 Heater shutdown emissions for NO_x and VOC are included in the Project emissions total.

PES TIER 3 PROJECT

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4.0 NEW SOURCE REVIEW APPLICABILITY

PES must comply with all federal and State require nents applicable to this proposed Project. The existing facility is a major stationary source for all criteria pollutants; therefore, the new sources in this Project must undergo a new source review analysis.

The PES Refining Complex is located in an area treated as severe nonattainment for ozone. It is designated as attainment for other pollutants. Because of the above designations, PES must evaluate the Project-related activities for the applicability of the NANSR program for VOC and NO_x as ozone precursors, and the applicability of the PSD program for NO₂, SO₂, CO, PM, PM₁₀, PM₂₅, H₂SO₄, and lead. Under the MANSR program, the Project is considered a major modification for ozone if the VOC or NO_x emissions exceed 25 TPY by itself or by aggregating with increases and decreases over the contemporaneous time period. Under PSD, a major modification occurs when NO₂ or SO₂ emissions exceed 40 TPY, CO emissions exceed 100 TPY, PM emissions exceed 25 TPY, PM₁₀ emissions exceed 7 TPY, or lead emissions exceed 0.6 TPY.

4.1 GREENHOUSE GAS TAILORING RULE

On 13 May 2010, EPA issued the final greenhouse gas (GHG) permitting rule officially known as the *Prevention of Significant Deterioration and Title V Greenhouse Gas Tailoring Rule* establishing GHGs as a PSD pollutant and setting major source emission thresholds for GHGs on a CO₂ equivalent (CO₂e) basis. If any new construction or modification of an existing facility results in a net emissions increase above established major source thresholds for GHGs on a CO₂e basis, GHG is considered a regulated pollutant for that project. Under the rule, GHG pollutants are considered to include carbon dioxide (CO₂), methane (CH₄), nitrous oxide (N₂O), hydrofluorocarbons (HFCs), perfluorocarbons (PFCs), and sulfur hexafluoride (SF₆).

ERM 17 PES TIER 3 PROJECT

On June 23, 2014 in Utility Air Regulatory Group v. EPA, the Supreme Court overturned part of EPA's trigger for when new or modified sources must seek permits for their GHG emissions, holding that the agency can only impose GHG PSD or Title V permitting when a facility's conventional emissions would otherwise trigger PSD or Title V. When PSD is triggered for conventional pollutants, GHG BACT will still be required if GHG emissions are above yet to be determined de minimis levels (75,000 ton/yr and 100,000 ton/yr threshold must be revisited).

Phase I of the rule was effective on 2 January 2011 and affects sources that are newly constructed or modified and are a "major source" under PSD for any pollutant other than GHGs. Upon triggering PSD for a non-GHG pollutant, the source must then determine PSD applicability for GHGs under the "Tailoring Rule" provisions. Under Phase I, newly constructed or modified facilities having a net increase of more than 75,000 TPY of CO₂e, would trigger PSD for GHGs.

As noted, the Supreme Court ruling indicates that a project's GHG potential emissions alone cannot trigger PSD permitting requirements. In the court's opinion, GHG BACT would only be required if PSD is triggered for a conventional pollutant first. Therefore, Phase II of the "Tailoring Rule" is no longer in effect.

4.2 PREVENTION OF SIGNIFICANT DETERIORATION ANALYSIS

The Prevention of Significant Deterioration regulations (40 CFR 52.21) are federal regulations that apply to new major sources or "major modifications" of existing "major stationary sources" located in attainment or unclassifiable areas for a given pollutant. The PSD regulations are enforced by AMS in accordance with 25 PA Code §127.81. The Philadelphia Refining Complex is a major stationary source, and a modification to the source that would result in a "significant emission increase" and a "significant net emissions increase" would trigger PSD applicability.

The PSD regulations define a major modification in 40 CFR 52.21(b)(3)(i) as any physical change in or change in the method of operation of a major stationary source that would result in a significant emission increase and a significant net emission increase of any pollutant subject to regulation under the Act. The regulation defines threshold levels of annual emission rates that constitute "significant increases" for a variety of pollutants. The PSD emissions analysis is performed as per applicable regulation in 25 PA Code §127.81 and 40 CFR §52.21.

In Step 1 of the analysis, the emissions increases from new sources are calculated. The emissions calculation methodology was described in the earlier sections. As indicated in **Table 4-1** below, CO_2e emissions for the proposed Project exceed the PSD threshold; however, because a conventional pollutant is not triggered, the CO_2e emissions are not subject to regulation under PSD.

Table 4-1 PSD Emissions Analysis (Step 1)

E talan	Pollutant (TPY)								
Emissions	NO ₂	SO ₂	со	PM	PM ₁₀	I'] vI _{2.5}	H ₂ SO ₄	Lead	CO₂e
PES Tier 3 Project	34.6	4.7	69.7	12.0	12.0	+7	0	8.3E-04	200,084
PSD Significant Level	40	40	100	25	15	.0	7	0.6	75,000
PSD Triggered (Before Netting Analysis)	No	No	No	No	No	No	No	No	No

4.3 NONATTAINMENT NEW SOURCE REVIEW AN LYSIS - OZONE

Facilities located in nonattainment areas that plan construction or modification of a source must evaluate the applicability of nonattainment NSR. The requirements are defined in 25 PA Code §127.201 through §127.217. Sources located in a nonattainment area, ozone transport region, or attainment or unclassifiable area impacting a nonattainment area are subject to permit requirements defined in 25 PA Code §127.203. In Pennsylvania, facilities located in the five county area including Philadelphia County are subject to the special permit requirements codified at §127.203. Under the special permit requirements, proposed new sources are subject to the NANSR requirements if the cumulative emissions calculated, using either one of the two scenarios below, equals or exceeds 25 tons per year of NO_x or VOC:

- Increases or decreases in emissions from the project are aggregated with other net emissions increases over the consecutive 5-calendar year period including the year in which the project is constructed; or
- Increases or decreases in emissions from the project are aggregated with other net emission increases or decreases over the previous 10-year period. In this case, the facility is subject only to the emissions offset requirements codified at §127.205.

If the resulting net change exceeds the applicable thresholds, those emissions must be offset by a ratio of 1.3 to 1. If the offsets come from internal emission reductions, then Lowest Achievable Emission Rate (LAER) requirement does not apply (25 PA Code §127.203(b)(3)).

Table 4-2 below presents a summary of Project emissions for NO_x and VOC aggregated with other net emissions increases over the consecutive 5-calendar year period including the year in which the Project construction is planned (calendar years 2011 through 2015). Contemporaneous Emissions Tables are provided in **Attachment D**.

Table 4-2 NANSR Netting Analysis for NO_x and VOC Emissions (5 calendar year)

Emissions	5 year NO _x (TPY)	5 year VOC (TPY)	
PES Tier 3 Project	11.2	6.7	
Contemporaneous Increases	12.8	13.2	
Net Emissions Increase	24.1	19.8	
NA-NSR Significance Level	25	25	
NA-NSR Review Required	No	No	

As shown in **Table 4-2** above, the 5 calendar year net emissions increases of NO_x and VOC from the proposed Project are below the NANSR threshold of 25 tons per year. Therefore, the proposed Project is not subject to the LAER requirements of 25 PA Code §127.205.

Table 4-3 below presents a summary of Project emissions for NO_x and VOC aggregated with other net emission increases or decreases over the previous 10 year period.

Table 4-3 NANSR Netting Analysis for NO_x and VOC Emissions (10 year)

Emissions	10 year NO _x (TPY)	10 year VOC (TPY)
PES Tier 3 Project	11.2	6.7
Contemporaneous Increases/Decreases	23.4	28.4
Net Emissions Increase	34.6	35.0
NANSR Significance Level	25	25
NANSR Review Required	Yes	Yes

As shown in **Table 4-3** above, the 10 year net emissions increases of NO_x and VOC from the proposed Project are above the NANSR applicability thresholds of 25 tons per year. Therefore, the proposed Project is subject to the offsetting requirements of 25 PA Code §127.205(3). PES plans to

surrender 45.0 tons of NO_x offsets (34.6 tons of NO_x emissions at a 1.3:1 ratio) and 45.5 tons of VOC offsets (35.0 tons of VOC emissions at a 1.3:1 ratio). PES is in active discussion with AMS regarding the accounting of emission reductions from the former Marcus Hook Refinery that were established while the facility was considered part of the Philadelphia Refining Complex. While PES believes the reductions should be considered contemporaneous reductions, for simplicity for the proposed Project, PES plans to use a portion of the remaining NO_x emission reduction credits (ERCs) generated from the shutdown of certain emissions sources at Marcus Hook to offset the 10 year net emissions increases of NO_x.

5.0 BAT DETERMINATION

In accordance with 25 PA Code §127.12, an applicant for Plan Approval must demonstrate that the emissions from a new source will be the minimum attainable through use of the Best Available Technology (BAT). BAT is defined as equipment, devices, methods or techniques as determined by the Department that will prevent, reduce or control emissions of air contaminants to the maximum degree possible and that are available or can be made available to the facility. 25 PA Code §121.1 (Definitions) defines a new source as a source that was constructed and commenced operation on or after July 1, 1972, or a source that was modified so that the fixed capital cost of new components exceeds 50% of the fixed capital cost that would be required to construct a comparable entirely new source.

The affected heaters in this proposed Project and their corresponding construction dates at the Complex are shown in **Table 5-1** below.

Table 5-1 Affected Heater Construction Dates

Heater	Construction Date		
Unit 864 PH-1 Heater	1971		
Unit 864 PH-7R Heater	To be installed		
Unit 864 PH-11 Heater	1971		
Unit 864 PH-12 Heater	1971		
Unit 870 H-1 Heater	2004		
Unit 870 H-2 Heater	2004		
Unit 870 H-3 Heater	To be installed		
Unit 1332 H-2 Heater	2005		
Unit 1332 H-3 Heater	1958		

The Unit 1332 H-3 Heater is excluded from this analysis because it was installed prior to July 1, 1972 and has not been modified since that date in any way that would result in the emission of an air contaminant not previously emitted. The Unit 870 H-1 Heater, Unit 870 H-2 Heater, and Unit 1332 H-2 Heater, all of which have ULNB installed, are excluded from this analysis because these sources were required to meet BAT at the time of installation and have not been modified since that date in any way that would result in the emission of an air contaminant not previously emitted.

While the Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12 heaters are planned to have LNB installed, the cost of this change will not be in excess of the 50% fixed capital cost described above for the Project to be considered a "new source" per 25 PA Code §121.1. The proposed replacement of the Unit 864 PH-7 Heater with an existing heater from the former Sunoco Inc. (R&M) Eagle Point Refinery and the proposed installation of the Unit 870 H-3 Heater are the only sources associated with the PES Tier 3 Project that are a "new source" per 25 PA Code §121.1.

PES has conducted a BAT analysis for the proposed Unit 864 PH-7R and Unit 870 H-3 Heaters. In this analysis PES reviewed information from various databases to determine recent requirements and emission limits for the new source associated with this Project, including:

- EPA's New Source Review website;
- U.S. EPA's RACT/BACT/LAER Clearinghouse 'RBLC') Database;
- Various state air quality regulations and websites;
- Recent EPA consent decrees within the refining industry; and
- State and federal guidance documents.

Note that BAT is a pollutant-specific determination. Based on a review of established emission control technologies and emission limits in permits, the following sections document the results of the source and pollutant specific BAT determinations.

5.1 NO_X CONTROLS

The Unit 864 PH-7R and Unit 870 H-3 Heaters will be equipped with ULNB that will achieve a NO_x emission rate of 0.02 lb/MMBtu and 0.03 lb/MMBtu, respectively. PES reviewed available and applicable NO_x controls that have been installed on process heaters at refineries or sim lar operations. The only additional NO_x control available beyond the controls planned is Selective Catalytic Reduction (SCR). The stack temperature of both the Unit 864 PH-7R and Unit 870 H-3 Heaters will be approximately 425 degrees Fahrenheit (°F) due to use of heat recovery in the stack that is integral to the process. According to the USEPA *Air Pollution Control Technology Fact Sheet* for SCR (EPA-452/F-03-032), the optimum operating temperature range for SCR is 480°F to 800°F. Therefore, the use of SCR on both the Unit 864 PH-7R and Unit 870 H-3 Heaters is not feasible.

Nonetheless, PES estimated the cost effectiveness for SCR for NO_x control in addition to the currently installed ULNB on the Unit 864 PH-7R and Unit 870 H-3 Heaters in the BAT NO_x cost effectiveness analysis presented in **Attachment** E. Cost effectiveness was calculated for SCR using the methodology in the regulations and in the "OAQPS Control Cost Manual" (EPA/452/B-02-001). Total annual costs are the sum of operating and maintenance (O&M) costs and capital recovery costs. The capital recovery costs assume the equipment will be amortized over a 20-year time frame at 20 percent interest, the rate PES uses for evaluating capital projects. Total capital required to implement SCR control and operating and maintenance costs were estimated using USEPA's Alternative Control Techniques Document - NO_x Emissions from Process Heaters (Revised) - EPA-453/R-93-034. The cost effectiveness of the additional SCR control on the Unit 864 PH-7R Heater is approximately \$137,000 per ton of NO_x emissions reductions, while the cost effectiveness of the additional SCR control on the Unit 870 H-3 Heater is approximately \$81,000 per ton of NO_x emissions reductions.

Accordingly, ULNB are considered BAT for the Unit 864 PH-7R and Unit 870 H-3 Heaters.

5.2 CO CONTROLS

The available emission controls for reducing CO emissions from process heaters include:

- Good combustion practices; and
- Oxidation catalysts.

Based on a review of the RBLC database and other permits issued for refineries, no documented cases of oxidation catalysts being implemented on similarly sized process heaters were identified. Therefore, installation of oxidation catalyst for heaters of this size has not been demonstrated and is not available. The lack of application in refineries is largely due to operational limitations of the oxidation catalysts. The installation of oxidation catalyst in flue gas containing more than trace levels of SO₂ will result in poisoning and deactivation of the catalyst by sulfur-containing compounds, as well as increasing the conversion of SO₂ to SO₃. This would increase condensable particulate matter emissions, which would foul the catalyst, in turn, prohibiting oxidation as well as increasing flue gas system corrosion rates.

Good combustion practice is the predominantly used control option for reducing CO emissions from process heaters. The use of combustion tuning and implementation of periodic maintenance on the process heaters ensure that the CO emissions are limited.

Accordingly, good combustion practices are BAT for limiting CO emissions from the Unit 864 PH-7R and Unit 870 H-3 Heaters

$PM/PM_{10}/PM_{2.5}$ CONTROLS

The available emission control options for reducing $PM/PM_{10}/PM_{2.5}$ emissions from process heaters include:

- Good combustion practices;
- Electrostatic precipitators;
- Baghouse or fabric filters; and
- Use of gaseous fuels.

Refinery fuel gas will be used as the only fuel for the Unit 864 PH-7R and Unit 870 H-3 Heaters. Based on our review of the RBLC database and permits issued at refineries, ESPs or baghouses are not installed on similarly sized heaters fired on refinery fuel gas. Though these control options are potentially technically feasible for combustion sources such as process heaters, they are not commercially demonstrated or similarly sized process heaters. Therefore, these control options are not further considered in this evaluation. The refinery fuel gas fired in the heaters is comprised of a significant amount of natural gas and therefore, is similar in heating value and characteristics to natural gas.

BAT for the Unit 864 PH-7R and Unit 870 H-3 Heaters for limiting PM/PM₁₀/PM_{2.5} emissions is good combustion practices and firing of refinery fuel gas.

5.4 SO₂ CONTROLS

The available emission control options for minimizing SO₂ emissions from process heaters includes:

Wet flue gas desulfurization (FGD) scrubber;

- · Dry FGD scrubber; and
- Use of gaseous fuels.

Based on a review of EPA's RBLC database, and permits issued for refineries, wet FGD and dry FGD systems have not been installed on natural gas or refinery fuel gas fired heaters at any refinery in the country. Though these control options are potentially technically feasible for combustion sources such as process heaters, they are not commercially demonstrated on similarly sized process heaters. Therefore, these control options are not considered further in this evaluation.

Refinery fuel gas consists of a combination of refinery process by-product gas and natural gas. The refinery by-product gas is desulfurized prior to supplementing with natural gas through a mix drum in order to ensure New Source Performance Standards Subpart J limits are met prior to combustion. Refinery fuel gas is used at every refinery in the country as part of balancing available energy from process operations and by-products.

The use of low sulfur refinery fuel gas is BAT for the Unit 864 PH-7R and Unit 870 H-3 Heaters for SO₂.

5.5 VOC CONTROLS

The available emission control options for minimizing VOC emissions from the process heaters includes:

- Oxidation catalysts; and
- Good combustion practices; and
- Use of gaseous fuels.

Based on our review of the RBLC databases, oxidation catalysts have not been demonstrated for VOC control on process heaters at refineries. The predominant control option to reduce VOC emissions from process heaters is the use of good combustion practices.

The Unit 864 PH-7R and Unit 870 H-3 Heaters will only fire refinery fuel gas which is lower in VOC content than liquid fuels and some other gaseous fuels. The Refinery removes many VOCs from the by-product gases before they are sent to the refinery fuel gas system and thus refinery fuel gas

consists of mostly non-VOC compounds such as methane, ethane, and hydrogen.

The use of good combustion practices and firing of refinery fuel gas is BAT for the Unit 864 PH-7R and Unit 870 H-3 Heaters for VOC.

6.0 APPLICABLE STANDARDS ANALYSIS

The following sections review the applicability of local, state, and federal regulations including National Emission Standards for Hazardous Air Pollutants (NESHAPS) and New Source Performance Standards (NSPS) to the PES Tier 3 Project.

6.1 AIR MANAGEMENT SERVICES REGULATIONS

AMS Regulations incorporate Pennsylvania air contaminant emissions limits and control efficiencies (Regulation I, Section X) and include by reference, the federal regulations (AMS Regulation 1, Section XI). AMS also regulates SO₂ emissions (Regulation III, Section II), fuel sulfur content (Regulation III, Section III), pump and compressor emissions (Regulation V, Section IV), and process equipment leaks (Regulation V, Section XIII).

With regard to Regulation VI, there will be no new air toxic contaminants associated with this Project.

There are no AMS regulations that are significantly different from, or more stringent than, the regulations cited herein. The proposed Project will not result in any additional AMS applicable requirements

6.2 FEDERAL NESHAPS (40 CFR PART 63)

The NESHAPS were promulgated after the 1990 Clean Air Act Amendments and require application of technology-based emissions standards for major and area sources of HAP. The PES hazardous air pollutant (HAP) emissions exceed 10 TPY for an individual HAP or 25 TPY for all HAP combined; therefore, it is considered a major source of HAPs.

Subpart DDDDD

The proposed PES Tier 3 Project is subject to the National Emission Standards for Hazardous Air Pollutants for Major Sources: Industrial, Commercial, and Institutional Boilers and Process Heaters (Boiler MACT) codified in 40 CFR 63.7490. The existing affected heaters must be in compliance with the Boiler MACT within 180 days of January 31, 2016 and new affected heaters within 180 days of initial startup. PES will demonstrate compliance by performing annual tune-ups of each affected heater and completing a one-time energy assessment for existing heaters.

6.3 FEDERAL NSPS (40 CFR PART 60)

Section 111 of the Clean Air Act authorized the EPA to develop technology based standards which apply to specific categories of stationary sources. These standards are referred to as New Source Performance Standards (NSPS). The following subsections highlight the requirements of the applicable NSPSs for the proposed Project.

6.3.1 Replacement Unit 864 PH-7R Heater

Subpart Ja is applicable to new or modified sources in petroleum refineries including: fluid catalytic cracking units (FCCU), fluid coking units (FCU), delayed coking units, fuel gas combustion devices, lares and sulfur recovery plants. The idle Unit 864 PH-7R Heater from the former Sunoco Inc. (R&M) Eagle Point Refinery was subject to NSPS Subpart Jat the commencement of operation (prior to the May 14, 2007 NSPS Subpart Ja applicability date) and continued to be subject to Subpart Jat the time when the Eagle Point Refinery was idled in the fourth quarter 2009.

Unlike the PSD and NANSR programs, reactivation of an idle source is not considered construction of a new source⁵. The replacement Unit 864 PH-7R Heater would only be subject to NSPS if the source has been modified or reconstructed, where 40 CFR 60.2 defines modification as...

"any physical change in, or change in the method of operation of, an existing facility which increases the amount of any air pollutant (to which a standard applies) emitted into the atmosphere by that facility or which results in the emission of any air pollutant (to which a standard applies) into the atmosphere not previously emitted."

The proposed changes to the Unit 864 Naphtha Hydrotreating Unit do not require physical changes or a change in the method of operation to the replacement Unit 864 PH-7R Heater which increases the amount of any pollutant to which a standard applies. Therefore, the replacement Unit 864 PH-7R Heater is considered subject to Subpart J and is not considered a modified source and therefore, not subject to Subpart Ja.

6.3.2 Unit 870 H-2 Heater

The Unit 870 H-2 Heater will have updated ULNBs installed as part of this Project. However, both the maximum firing capacity (MMBtu/hr) and NO_x

Memo from Edward E. Reich, Dir., Div. Of Stationary Source Enf., to Sandra S. Gardebring, Dir., Region V Enf. Div. (Oct. 30, 1980).

emission rate (lb/MMBtu) of the Unit 870 H-2 Heater will be unaffected by the change. The proposed physical change to the Unit 870 H-2 Heater will not result in increases the amount of any pollutant to which a standard applies. Therefore, the Unit 870 H-2 Heater is considered subject to Subpart J and is not considered a modified source and therefore, not subject to Subpart Ja.

6.3.3 New Unit 870 H-3 Heater

The new Unit 870 H-3 Heater is considered a fuel gas combustion device and is subject to Subpart Ja, which includes sulfur and NO_x standards. As per 40 CFR 60.107a(2), PES complies with the hydrogen sulfide (H₂S) concentration limits in 60.102a(g)(1)(ii) by continuously monitoring and recording the concentration by volume (dry basis) of H₂S in the refinery fuel gas system.

 NO_x emissions limitations apply to natural draft process heaters with a rated capacity greater than 40 MMBtu/hr. The Unit 870 H-3 Heater will subject to the NO_x limit found at 40 CFR §60.102a(g)(2)(i)(B) which is 0.040 lb/MMBtu on a 30-day rolling average basis. The expected NO_x emission rate for the Unit 870 H-3 Heater is 0.03 lb/MMBtu.

As per 40 CFR $\S60.107a(d)$, PES will be required install, operate, calibrate and maintain an instrument for continuously monitoring and recording the concentration (dry basis, 0-percent excess air) of NO_x emissions into the atmosphere to comply with the NO_x emissions limit in 40 CFR $\S60.102a(g)(2)(i)(B)$. The monitor must also include an oxygen monitor for correcting the data for excess air.

6.3.4 Other Affected Heaters

PES evaluated whether the affected heaters that are experiencing increased utilization (Unit 864 PH-1 Heater, Unit 864 PH-11 Heater, Unit 864 PH-12 Heater, Unit 870 H-1 Heater, and Unit 1332 H-2) as part of the PES Tier 3 Project trigger the applicability of NSPS for affected sources.

The proposed changes to the Unit 864 Naphtha Hydrotreating Unit, Unit 870 LSG Unit, or Unit 1332 Reformer Unit do not require physical changes or capital expenditures on the affected facility (i.e., the heaters) to accommodate the increased utilization. As such, no sources are considered to be modified sources under USEPA's New Source Performance Standards codified under 40 CFR Part 60. Specifically, 40 CFR 60.14(e)(2) excludes from the definition of modification...

"an increase in production rate of an existing facility, if that increase can be accomplished without a capital expenditure on that facility."

The increase in heater utilization sought in this Project represents a production rate increase for the affected heaters. All of the heaters serve the same overall purpose - to produce heated hydrocarbon streams for processing. Additionally, as discussed in published USEPA guidance, both changes in production rate and operating changes are included in the assessment of capital expenditure associated with the project.

The increase in utilization of the affected heaters in this Project can be achieved without any capital expenditure. Therefore, the affected heaters are not considered modified sources and therefore are not subject to NSPS.

ERM 31 PES TIER 3 PROJECT

⁶ EPA, 1989. Re: Applicability of NSPS. Letter from Don R. Clay, Acting Assistant EPA Administrator of EPA to Mr. John W. Boston, WEPCO, February 15, 1989.

Attachment A AMS Plan Approval Application Forms



CITY OF PHILADELPHIA

DEPARTMENT OF PUBLIC HEALTH PUBLIC HEALTH SERVICES AIR MANAGEMENT SERVICES Air Management Services 321 University Avenue Philadelphia PA 19104-4543 Phone: (215) 685-7572 FAX: (215) 685-7593

APPLICATION FOR PLAN APPROVAL TO CONSTRUCT, MODIFY DR REACTIVATE AN AIR CONTAMINATION SOURCE AND/OR AIR CLEANING DEVICE

(Prepare all information completely in print or type in triplicate) SECTION A - APPLICATION INFORMATION Location of source (Street Address) Facility Name 3144 Passyunk Avenue Philadelphia Energy Solutions Refining and Marketing LLC Owner Tax ID No Philadelphia Energy Solutions Refining and Marketing LLC 61-1689574 Mailing Address Telephone No. Fax No. 3144 Passyunk Avenue (215) 339-2074 (215) 339-2657 Contact Person Charles D. Barksdale Jr. Manager, Environmental Department Mailing Address Telephone No. Fax No 3144 Passyunk Avenue Philadelphia, PA 19145 (215) 339-2074 (215) 339-2657 E-mail Address CHARLES.BARKSDALE@pes-companies.com SECTION B - DESCRIPTION OF ACTIVITY Application type SIC Code Completion Date January 1, 2017 Applicable requirement

☑ NSPS ☑ NESHAP ☐ Case by Case MACT ☑ NSR ☐ PSD Does Facility submit Compliance Review Form biannually? Yes □ No If No attach Air Pollution Control Act Compliance Review Form with this application. PES plans to reconfigure existing process units, re-route intermediate process streams, and expand hydrotreating process capacity to enable compliance with the Tier 3 gasoline standards. This includes the installation of low NOx burners (LNB) on the Unit 864 PH-1, Un t 864 PH-11, Unit 864 PH-12 refinery fuel gas fired heaters; replacement of the Unit 864 PH-7 Heater with an idle heater from the former Sunoco Inc. (R&M) I agle Point Refinery; and installation of a new Unit 870 H-3 Heater. For the purposes of this application, the project is referred to as the "PES Tier 3 Project". SECTION C - PERMIT COORDINATION (ONLY REQUIRED FOR LAN) DEVELOPMENT) Ouestion YES NO 1. Will the project involve construction activity that disturbs five or more acres of land? X 2. Will the project involve discharge of industrial wastewater or stormwater to a dry swale, surface water, ground water > an existing sanitary sewer X system? 3. Will the project involve the construction and operation of industrial waste treatment facility? X 4. Is onsite sewage disposal proposed for your project? X 5. Will the project involve construction of sewage treatment facilities, sanitary sewer, or sewage pumping station? X 6. Is a stormwater collection and discharge system proposed for this project? X 7. Will any work associated with this project take place in or near a stream, waterway, or wetland? X X 8. Does the project involve dredging or construction of any dam, pier, bridge or outfall pipe? 9. Will any solid waste or liquid wastes be generated as a result of the project? X 10. Is a State Park located within two miles from your project? X SECTION D - CERTIFICATION I certify that I have the authority to submit this Permit Application on behalf of the applicant named herein and that the information provided in this application is tryog and correct to the best of my knowledge and information. 3144 Passyunk Avenue, Philadelphia, PA 19145 Phone 215-339-7440 Fax 215-339-2657 Central Engineering Pickerina SECTION E - OFFICIAL USE ONLY Plant ID Application No. Health District Census Tract Date Received 0150 Conformance by

AMS Rev 10/96 Page _2_ of _18_

					SECTION	F 1 - GENERAL S	SECTION F 1 - GENERAL SOURCE INFORMATION	N							
	1. SOURCE							7.	AL PROCESS	NORMAL PROCESS OPERATING SCHEDULE	SCHE	OULE			
		Y		B.	C.	D.	ம	.A		B. C.			D.		
_		Type Source	Manu	Manufacturer	Model No.	Rated Capacity	Type of Materials Processed			_		6 Throu	% Throughput/Quarter	Quarter	
		(Describe)	ofs	of Source		(Specify units)		Processed/yr. (Specify units)	_	hr/day hr/yr					
											I st	2 nd		3rd '	4 th
-	Unit 864 F	Unit 864 PH-7R Heater	N/A		N/A	70.0 MMBtu/hr									
	(See attac	(See attached report)											_	-	
7	Unit 864 F	Unit 864 PH-1 Heater	N/A		N/A	74.9 MMBtu/hr									
	(See attac	(See attached report)									4	4	4	+	
8	Unit 864 F	Unit 864 PH-11 Heater	N/A		N/A	74.0 MMBtu/hr									
	(See attac	(See attached report)									_	_	\dashv	+	
4	Unit 864 F	Unit 864 PH-12 Heater	N/A		N/A	85.1 MMBtu/hr									
	(See attac	(See attached report)											+	+	
S	Unit 870 I	Unit 870 H-3 Heater	N/A		N/A	110.0 MMBtu/hr									
	(See attac	(See attached report)									_	_	\dashv	+	
9	See attach	See attached report for affected													
	sources.										_	4	4	\dashv	Ì
3.	ESTIMAT	3. ESTIMATED FUEL USAGE (Specify Units)	ify Units)					4. ANNUAL FUEL USAGE	USAGE						
A. U	A. Used in	B.	C.	D.	Ë	шi	G.	Y.	B.	ن			D.		
'n	Unit	Type Fuel	Average	Maximum	Percent	Percent Ash	Heating Value	Annual Amounts	Average	Total hr/yr	_	F .	// #a-q-0.	10.0	
			Hourly	Hourly Rate	Sulfur)		hr/day			% 11EO	/o 11ii Ougiipuv Çuai tei	Zuan ter	
			Rate											-	
											l st	2 nd		3rd	4 ^t
Unit 864		Refinery Fuel Gas		70.0			1028 Btu/scf		24 hr/day	0928	-				
PH-7R Heater				MMBtu/hr						hr/yr					
Unit 864 PH-1		Refinery Fuel Gas		74.9			1028 Btu/scf		24 hr/day	8760					
Heater				MMBtu/hr						hr/yr			-	+	
Unit 864		Refinery Fuel Gas		74.0			1028 Btu/scf		24 hr/day	8760					
PH-11 Heater	Heater			MMBtu/hr						hr/yr		4	\dashv	-	
Unit 864		Refinery Fuel Gas		85.1			1028 Btu/scf		24 hr/day	8760					
PH-12 Heater	Heater			MMBtu/hr						hr/yr			\dashv	\dashv	
Unit 870 H-3	0 H-3	Refinery Fuel Gas		110.0			1028 Btu/scf		24 hr/day	8760					
Heater				MMBtu/hr						hr/yr		_	+	1	
	S	See attached report for													
	æ	affected sources.									_	_	\dashv	\dashv	
S. IMP	5. IMPORTANT:	Attach on a separate sl	heet a flow di	iagram of proce	ss giving all (ga	seous, liquid, and so	Attach on a separate sheet a flow diagram of process giving all (gaseous, liquid, and solid) flow rates. Also list raw materials charged to process equipment and the amounts charged	w materials charg	ed to process	equipment a	nd the ar	nounts	charge	eq.	
		(tons/hour, etc.) at ra	ted capacity	(give maximum	, minimum and	average charges des	(tons/hour, etc.) at rated capacity (give maximum, minimum and average charges describing fully expected variations in production rates). Indicate (on diagram) all points where	ations in productio	n rates). Ind	icate (on diag	;ram) all	points	where		
		contaminants are controlled (location of water sprays, hoods or other pickup points, etc.).	strolled (loca)	tion of water sp	rays, hoods or e	ther pickup points, t	itc.).								

SECTION F 1 - GENERAL SOURCE INFORMATION, CONTINUED
6. Describe process equipments in detail.
Relevant process equipment include refinery fuel gas fired heaters, a recirculating cooling tower, the U sit 867 Sulfur Recovery Unit, and
fugitive emission components.
See the attached report for additional details.
7. Describe fully the methods used to monitor and record all operating conditions that may affect the emission of air contaminants. Provide detailed information to show that these methods provided are adequate.
PES will be replacing the existing Unit 864 PH-7 heater (nominal firing duty of 45.0 MMBtu/hr) with an existing idle heater (LSG H-1) located at the former Sunoco Inc. (R&M) Eagle Point Refinery in New Jersey. The replacement heater will be designated Unit 864 PH-7R. This replacement heater is equipped with ULNB that will achieve a NO _x emission rate of 0.02 lb/MMBtu. PES will also be installing a
new refinery fuel gas fired heater designated Unit 870 H-3 (nominal firing duty of 110.0 MMBtu/h·) and will be equipped with ULNB that will achieve a NO _x emission rate of 0.03 lb/MMBtu. Lastly, as part of the Project, PES has elected to install LNB on the Unit 864 PH-1, Unit 864 PH-11, and Unit 864 PH-12 heaters that will achieve a NO _x emission rate of 0.06 lb ↑ 1MBtu.
See the attached report for additional details.
See the attached report for additional details.
8. Describe modifications to process equipments in detail.
See the attached report for additional details.
9. Attach any and all additional information necessary to adequately describe the process equipment and to perform a thorough evaluation of the extent and nature of its emissions.
See the attached report that includes a BAT analysis.

- Provide equipment information on this page if sources do not belong to special categories in F2 to F8, otherwise remove this page from this application. If there are more equipment, copy this page and fill in the information as indicated

	SECTION F 2	COMBUSTION UNIT	S INFORMATIO	N	
1. COMBUSTION UNITS - See the attac	ched report sections.				
A. Manufacturer		B. Model No.		C. Unit No.	
Not applicable		Not applicable		Unit 864 PH-7R H	leater
D. Rated heat input (Btu/hr)		E. Peak heat input (Btu.	/hr)	F. Use	-
70.0 MMBtu/hr				Process heat	
G. Method firing	_		_		_
☐ Pulverized ☐ Spreader Stoker [Cyclone Tangenti	al Mormal Fluidized	bed Other		
2. FUEL REQUIREMENTS					
ТҮРЕ	<i>QUANTITY</i> <i>HOURLY</i>	QUANTITY ANNUALLY	SULFUR	ASH	BTU CONTENT
OIL NUMBER	GPH at 60 ° F	x10 ³ Gal.	% by wt.	% by wt.	Btu/Gal. & lbs/Gal. @ 60°F
		x10 ⁶ SCF	gr/100		
NATURAL GAS OTHER	68.1 MSCFH	_	SCF 162 ppmv H ₂ S		Btu/SCF 1,028 Btu/SCF
Refinery Fuel Gas			maximum		1,028 BlWSCF
3. COMBUSTION AIDS, CONTROLS, A	AND MONITORS				
A. Overfire jets	_	Туре	Number		Height above grate
B. Draft controls		Туре			
C. Oil preheat	-	_			
D. Soot cleaning		Temperature (°F)	Frequency		
E. Stack sprays		Method			
☐ F. Opacity monitoring device	_		Method	_	Cost
G. Sulfur oxides monitoring device		Туре	Method		Cost
H. Nitrogen oxides monitoring device		Туре	Method		Cost
☐ I. Fuel metering and/or recording device	ees	Туре	Method		Cost
J. Atomization interlocking device		Type Method			Cost
K. Collected flyash reentrainment previous	entative device	Туре			
L. Modulating controls	ton				
A	utomatic	_			
4. Flyash reinjection. (Describe operati	on)				
5. Describe method of supplying make up	air to the furnace room.				
•					
Section F 2 - Combustion Units Info	rmation, Continued				

- Use this page for Degreaser, otherwise remove this page from this application. If you have more units, copy this page and fill in the information as indicated

6.	OPERATING SCHEDUL	.E				
	24	hours/day		days/week	<u>52</u>	weeks/year
-	SEASONAL DEDIODS (AONTHE				
7.	SEASONAL PERIODS (1	MONTHS)				
	Operating using primary f	uel		Operating us	ing secondary fuel	
			-			
ļ		_ to	_		to	
	Non-operating					
		•				
		to				
8.	If heat input is in excess o	f 250 x 10 6 Btu/hr., describe	e fully the methods u	sed to record the following	g: rate of fuel burne	cd; heating value, sulfur and ash content of
	; smoke, sulfur oxides and i ration rate.	nitrogen oxides emissions; an	nd if electric generati	ng plant, the average elect	rical output ar d the	minimum and maximum hourly
5****						
		record, and report with ap	plicable requireme	nts found in the Philadel	phia Refinen, 's exi	sting Title V permit and the Consent
Dec	ree.					
9.	Describe modifications to	boiler in detail.				
See	the attached report section	ıs.				
10.	Type and method of dispo	osal of all waste materials gen	erated by this boiler			
	(Is a Solid Waste Disposa	l Permit needed? Yes	No)			
,,	Daiofferdana Trada and	od of handling the waste water	- from this bailer an	d its associated air nollistic	on control cause man	at .
11.		gement Permit needed?		d its associated air poliution	on control equit men	и.
	(15 a Water quarty Mariag	content remark needed.	<u> </u>			
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ĺ						
12.	Attach any and all addition	nal information necessary to	perform a thorough	evaluation of this boiler.		
See	the attached report section	ns.				
	and a port section					
l.						

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	SECTION F 2 -	COMBUST	ION UNIT	S INFORMATION	N	
1. COMBUSTION UNITS - See the attack	ched report sections.					
A. Manufacturer		B. Model I	No.		C. Unit No.	
Not applicable		Not applicab	le		Unit 864 PH-1 Hea	iter
D. Rated heat input (Btu/hr)		E. Peak he	at input (Btu/	hr)	F. Use	
74.9 MMBtu/hr					Process heat	
G. Method firing		_		_		
☐ Pulverized ☐ Spreader Stoker [Cyclone Tangenti	al 🛛 Normal	Fluidized	bed Other		
2. FUEL REQUIREMENTS						
ТҮРЕ	QUANTITY HOURLY	QUAN ANNUA	TITY 4LLY	SULFUR	ASH	BTU CONTENT
OIL NUMBER	CDI -4					Btu/Gal. &
	GPH at 60 ⁰ F		x10 ³ Gal.	% by wt.	% by wt.	lbs/Gal. @ 60°F
			x10 ⁶ SCF	gr/100		
NATURAL GAS	SCFH			SCF		Btu/SCF
OTHER Refinery Fuel Gas	72.9 MSCFH			162 ppmv H₂S maximum		1,028 Btu/SCF
3. COMBUSTION AIDS, CONTROLS, A	AND MONITORS					
A. Overfire jets		Туре		Number		Height above grate
B. Draft controls		Туре				
C. Oil preheat						
D. Soot cleaning		Temperature	e (°F)	Frequency		
☐ E. Stack sprays		Method				
☐ F. Opacity monitoring device				Method		Cost
G. Sulfur oxides monitoring device		Type Method		Method		Cost
☐ H. Nitrogen oxides monitoring device		Type Method			Cost	
1. Fuel metering and/or recording device	ces	Type Method			Cost	
☐ J. Atomization interlocking device		Type Method			Cost	
☐ K. Collected flyash reentrainment prev	entative device	Туре				
L. Modulating controls S	Step					
4. Flyash reinjection. (Describe operati	ion)					
5. Describe method of supplying make up	air to the furnace room.					

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		SECTION F 2 - C	OMBUSTION	UNITS INFORMATI	ON, CONT	INUED		
6.	OPERATING SCHEDUL	E						
	24	hours/day	7	days/week	52	weeks/year		
7.	SEASONAL PERIODS (MONTHS)						
	Operating using primary f	uel		Operating us	ing secondary f	fuel		
		to				0		
				n-operating				
				-				
				to				
8.	If heat input is in excess of fuels; smoke, sulfur oxide generation rate.	of 250 x 10 ⁶ Btu/hr., describe es and nitrogen oxides emissi	fully the methods upons; and if electric	ised to record the following generating plant, the ave	ng: rate of fue rage electrical	burned; heating value, sulfur and ash content of output and the minimum and maximum hourly		
PES Deci		record, and report with a	pplicable requiren	ents found in the Phila	delphia Refine	ry's existing Title V permit and the Consent		
ļ								
9.	Describe modifications to	boiler in detail.						
See	the attached report section							
	are accuered report section							
10.	Type and method of dispo (ls a Solid Waste Disposal	sal of all waste materials gene	erated by this boiler No)					
	(is a some waste Disposal	reminenceded res	110)					
11.	Briefly describe the metho	od of handling the waste water	r from this boiler an	d its associated air pollution	on control equi	ment.		
	(Is a Water quality Manag	ement Permit needed? Y	es 🛛 No)					
12.	Attach any and all addition	nal information necessary to	perform a thorough	evaluation of this boiler				
1	-		Actorni a utorougii	evaluation of this boller.				
See	the attached report section	18.						

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	SECTION F 2 -	COMBUS	STION UNIT	S INFORMATION	N	
1. COMBUSTION UNITS - See the attac	ched report sections.					
A. Manufacturer		B. Mod	el No.		C. Unit No.	
Not applicable		Not applic	able		Unit 864 PH-11 He	eater
D. Rated heat input (Btu/hr)		E. Peak	heat input (Btu/	/hr)	F. Use	
74.0 MMBtu/hr					Process heat	
G. Method firing						
☐ Pulverized ☐ Spreader Stoker [Cyclone Tangenti	al 🛭 Norm	al Fluidized	bed Other		
2. FUEL REQUIREMENTS						
TYPE	QUANTITY HOURLY		ANTITY IUALLY	SULFUR	ASH	BTU CONTENT
OIL NUMBER			_			D. 10.1.0
	GPH at 60 ⁰ F		x 10 ³ Gal.	% by wt.	% by wt.	Btu/Gal. & lbs/Gal. @ 60°F
			x10 ⁶ SCF	gr/100		 _
NATURAL GAS	SCFH		X10 SC1	SCF		Btu/SCF
OTHER Refinery Fuel Gas	72.0 MSCFH			162 ppmv H ₂ S maximum		1,028 Btu/SCF
3. COMBUSTION AIDS, CONTROLS, A	AND MONITORS					
A. Overfire jets		Туре		Number		Height above grate
B. Draft controls		Туре				_
C. Oil preheat						
D. Soot cleaning		Temperat	ure (° F)	Frequency		
E. Stack sprays		Method				
☐ F. Opacity monitoring device				Method		Cost
G. Sulfur oxides monitoring device		Туре		Method		Cost
☐ H. Nitrogen oxides monitoring device				Method		Cost
☐ I. Fuel metering and/or recording devic	es			Method		Cost
J. Atomization interlocking device		Type Method			Cost	
☐ K. Collected flyash reentrainment preve	entative device	Туре				
L. Modulating controls S	tep utomatic					
4. Flyash reinjection. (Describe operation)	on)					
5. Describe method of supplying make up	air to the furnace room.					

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	_	SECTION F 2 - C	OMBUSTION	UNITS INFORMATI	ON, CONT	INUED
6.	OPERATING SCHEDULE	E				
	24	hours/day	7	days/week	52	weeks/year
7.	SEASONAL PERIODS (M	1ONTHS)				
	Operating using primary fu	uel		Operating us	ing secondary	fuel
		to				to
			No	n-operating		
				to		
				10		
8.	fuels; smoke, sulfur oxides generation rate.	s and nitrogen oxides emission	ons; and if electric	generating plant, the ave	rage electrica	burned; heating value, sulfur and ash content of output and the minimum and maximum hourly
PES Deci		record, and report with ap	oplicable requiren	nents found in the Phila	delphia Refir	ery's existing Title V permit and the Consent
Deci	ес.					
9.	Describe modifications to b	boiler in detail.		_		·
See	the attached report sections	s.				
		•				
10.		sal of all waste materials gene	rated by this boiler			
	(ls a Solid Waste Disposal	Permit needed? Yes	⊠ No)			
ļ.,.	B. (4.1)	1.61 111 2				
11.	(Is a Water quality Manage	d of handling the waste water ement Permit needed? Ye	from this boiler an es \overline{\overline{No}}	d its associated air pollution	on control ecu	ipment.
12.	Attach any and all addition	nal information necessary to p	erform a thorough	evaluation of this boiler.		
	the attached report sections					
366	are arraculou report sections	>•				

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	SECTION F 2 -	COMBUSTION UNIT	S INFORMATION	N	
1. COMBUSTION UNITS – See the atta	ched report sections.		-		
A. Manufacturer		B. Model No.		C. Unit No.	<u> </u>
Not applicable		Not applicable		Unit 864 PH-12 H	eater
D. Rated heat input (Btu/hr)		E. Peak heat input (Btu	/hr)	F. Use	
85.1 MMBtu/hr				Process heat	
G. Method firing					
☐ Pulverized ☐ Spreader Stoker	☐ Cyclone ☐ Tangenti	ial 🛛 Normal 🗌 Fluidized	bed Other		
2. FUEL REQUIREMENTS					
ТҮРЕ	QUANTITY HOURLY	QUANTITY ANNUALLY	SULFUR	ASH	BTU CONTENT
OIL NUMBER					
	GPH at 60 °F	x 10 ³ Gal.	% by wt.	% by wt.	Btu/Gal. & lbs/Gal. @ 60°F
		x10 ⁶ SCF	gr/100		
NATURAL GAS	SCFH	XIO SCI	SCF		Btu/SCF
OTHER Refinery Fuel Gas	82.8 MSCFH		162 ppmv H ₂ S maximum		1,028 Btw/SCF
3. COMBUSTION AIDS, CONTROLS, A	LAND MONITORS		- maximum		
A. Overfire jets		Туре	Number		Height above grate
		-7F-			
B. Draft controls		Туре			
C. Oil preheat					
D. Soot cleaning		Temperature (°F)	Frequency		
☐ E. Stack sprays		Method			
F. Opacity monitoring device			Method		Cost
G. Sulfur oxides monitoring device		Туре	Method		Cost
H. Nitrogen oxides monitoring device		Туре	Method		Cost
☐ I. Fuel metering and/or recording device	ces	Туре	Method		Cost
J. Atomization interlocking device		Type Method			Cost
K. Collected flyash reentrainment prev	ventative device	Туре			
L. Modulating controls	Step				
□ A	Automatic				
4. Flyash reinjection. (Describe operat	ion)				
5. Describe method of supplying make up	o air to the furnace room.				

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		SECTION F 2 - C	COMBUSTION	UNITS INFORMAT	ION, CONTINU	ED			
6.	OPERATING SCHEDUI	Æ							
	24	hours/day		days/week	52	weeks/year			
7.	SEASONAL PERIODS (MONTHS)							
	Operating using primary	fuel	_	Operating us	ing secondary fuel				
		_ to							
				n-operating					
				to					
8.	If heat input is in excess of fuels; smoke, sulfur oxid generation rate.	of 250 x 10 ⁶ Btu/hr., describe es and nitrogen oxides emiss	e fully the methods usions; and if electric	used to record the following enerating plant, the average	ng: rate of fue burne rage electrical output	ed; heating value, sulfur and ash content of it and the minimum and maximum hourly			
PES	will continue to monitor	, record, and report with a	pplicable requirem	ents found in the Phila	delphia Refinery's	existing Title V permit and the Consent			
Deci	ee.								
ĺ									
9.	Describe modifications to	boiler in detail.							
1	he attached report section								
	и протовение								
}									
10	T 1 d 1 C I	1.6.11	11 4:1 7						
10.	(Is a Solid Waste Disposa	osal of all waste materials gen I Permit needed? Yes	erated by this boiler. No)						
									
11.	(Is a Water quality Manag	od of handling the waste wate gement Permit needed? \(\sime\) Y	r from this boiler and es 🔲 No)	d its associated air polluti	on control equipmen	t.			
12.	Attach any and all addition	onal information necessary to	perform a thorough	evaluation of this boiler.					
See	he attached report section	ns.							

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- If you have more units, copy this page and fill in the information as indicated

	SECTION F 2 -	COMBUSTION UNIT	S INFORMATIO	N	
1. COMBUSTION UNITS - See the attac	ched report sections.				
A. Manufacturer		B. Model No.		C. Unit No.	
Not applicable		Not applicable		Unit 870 H-3 Heat	er
D. Rated heat input (Btu/hr)		E. Peak heat input (Btu	ı/hr)	F. Use	
110.0 MMBtu/hr				Process heat	
G. Method firing					
☐ Pulverized ☐ Spreader Stoker [Cyclone Tangenti	ial 🛛 Normal 🗌 Fluidized	i bed Other		
2. FUEL REQUIREMENTS					
ТҮРЕ	QUANTITY HOURLY	QUANTITY ANNUALLY	SULFUR	ASH	BTU CONTENT
OIL NUMBER	OPU				D: /0.1.0
	GPH at 60 ⁰ F	x10 ³ Gal.	% by wt.	% by wt.	Btu/Gal, & lbs/Gal. @ 60°F
NATURAL GAS	SCFH	x10 ⁶ SCF	gr/100 SCF		Btu/SCF
OTHER Refinery Fuel Gas	107.0 MSCFH		162 ppmv H ₂ S maximum		1,028 Btu/SCF
3. COMBUSTION AIDS, CONTROLS, A	AND MONITORS		- Indamen		
A. Overfire jets		Туре	Number		Height above grate
B. Draft controls		Туре			
C. Oil preheat					
D. Soot cleaning		Temperature (°F)	Frequency		
☐ E. Stack sprays		Method			
F. Opacity monitoring device			Method		Cost
☐ G. Sulfur oxides monitoring device		Туре	Method		Cost
H. Nitrogen oxides monitoring device		Type – CEMS	Method - Chemilu	minescence	Cost
☐ 1. Fuel metering and/or recording device	es	Type Method			Cost
☐ J. Atomization interlocking device		Type Method		Cost	
K. Collected flyash reentrainment preven	entative device	Туре			
L. Modulating controls S	tep utomatic				
4. Flyash reinjection. (Describe operation)	on)				
5. Describe method of supplying make up	air to the furnace room.				-

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	SECTIO	ON F 2 - COMBUSTION	UNITS INFORMATI	ON, CONT	INUED
6.	OPERATING SCHEDULE				
	hours/da	<u> </u>	days/week	52	weeks/year
7.	SEASONAL PERIODS (MONTHS)				
	Operating using primary fuel		Operating usi	ng secondary	fuel
	to				to
			on-operating		
		IN.			
			to	_	
8.	If heat input is in excess of 250 x 10 ⁶ Btu fuels; smoke, sulfur oxides and nitrogen of generation rate.	hr., describe fully the methods oxides emissions; and if electri	used to record the followin c generating plant, the aver	g: rate of fue rage electrical	burned; heating value, sulfur and ash content of output and the minimum and maximum hourly
		port with applicable require	ments found in the Philad	lelphia Refin	ery's existing Title V permit and the Consent
Dec	ree.				
l					
9.	Describe modifications to boiler in detail.				
'	the attached report sections.				
366	the attached report sections.				
]					
10.	Type and method of disposal of all waste n	naterials generated by this boile	er.		-
	(Is a Solid Waste Disposal Permit needed?	☐ Yes No)			
					· — — — — — — — — — — — — — — — — — — —
I 1.	Briefly describe the method of handling the (Is a Water quality Management Permit ne	e waste water from this boiler a eded? Yes No)	and its associated air pollution	on control equ	i) ment.
12.	Attach any and all additional information r	necessary to perform a thorough	h evaluation of this boiler.		··
	the attached report sections.				
See	the attached report sections.				

- Use this page for Degreaser, otherwise remove this page from this application. If you have more units, copy this page and fill in the information as indicated

SECTION G - FLUE AND AIR	CONTAMINANT EMISSION IN	FORMATION	
I. STACK AND EXHAUSTER			
Unit 864 PH-7R Heater Stack			
A. Outlet volume of exhaust gases	B, Exhauster (attach fan curve	s)	
CFM @% Moisture	in w.g	HP @	RPM
C . Stack height above grade (ft) 152.5	D Stack diameter (ft) or Outlet duct a	rea (sq. ft.)	E Weather Cap
Grade elevation (ft)	5.92 feet (71 inches)		☐ YES ☒ NO
Distance from discharge to nearest property line(ft)			
F. Indicate on an attached sheet the location of sampling ports with respect	to exhaust fan, breeching, etc. Give all	necessary dimensions.	
To be determined.			
2 POTENTIAL PROCESS EMISSIONS (OUTLET FROM PROCESS, BE	EFORE ANY CONTROL EQUIPMENT	()	
See the attached report sections.			
A. Particulate loading (lbs/hr or gr/DSCF) B. Specific gravity of	of particulate (not bulk density)	C . Attached particle size	distribution information
D. Specify gaseous contaminants and concentration			
Contaminant Concentration VOC Contam	ninants Concentration		
(1) SO _x ppm (Vol.)lbs/hr (4)	ppm (Vol.)	lbs/hr	
(2) NO _x ppm (Vol.)lbs/hr (5)	ppm (Vol.)	lbs/hr	
(3) CO ppm (Vol.) lbs/hr (6)	ppm (Vol.)	lbs/hr	
E. Does process vent through the control device? YES NO			
- If YES continue and fill out the appropriate SECTION H - CONTROL I - If NO skip to SECTION I - MISCELLANEOUS INFORMATION	EQUIPMENT		
F. Can the control equipment be bypassed: (If Yes, explain) YE	S 🔯 NO		
3. ATMOSPHERIC EMISSIONS			
A. Particulate matter emissions (lbs/hr or gr/DSCF)			
See the attached report sections.			
B. Gaseous contaminant emissions			
Contaminants Concentration VOC Cont	aminants Concentration		
(1) SO _X ppm (Vol.) lbs/hr (4)	ppm (Vol.)	lbs/hr	
(2) NO _X ppm (Vol.)lbs/h (5)			nr
(3) CO ppm (Vol.) lbs/h) (6)	ppm (Vol.)	lbs/hr	
See the attached report sections.			

SECTION H - CONTROL EQUIPMENT, CONTINUED
12. COSTS – See the attached report sections.
A. List costs associated with control equipment. (List individual controls separately)
Control Equipment Cost:
Direct Cost:
Indirect Cost:
B. Estimated annual operating costs of control equipment only.
13. Describe modifications to control equipment in detail.
Not applicable.
14. Describe in detail the method of dust removal from the air cleaning and methods of controlling fugitive emissions from lust removal, handling and disposal.
Not applicable.
15. Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If so, describe.
Not applicable.
16. Attach manufacturer's performance guarantees and/or warranties for each of the major components of the control system (or complete system).
17. Attach the maintenance schedule for the control equipment and any part of the process equipment that if in disrepair we ild increase the air contaminant emissions. Periodic maintenance reports are to be submitted to the Department.
Maintenance will continue to be provided as per the manufacturer's recommendations and the Title V Permit.
18. Attach any and all additional information necessary to thoroughly evaluate the control equipment.
See the attached report sections.

- Provide control equipment information on this page if it pertains to this application, otherwise remove this page from the application. If there are more of the same type of control equipment, copy that page and fill in the information as indicated. Control equipment can be found from a manufacturer catalogue or vendors.

SECTION G - FLUE AND AIR	CONT	AMINANT EMISSION I	NFORMATION		
1. STACK AND EXHAUSTER Unit 870 H-3 Heater Stack					
A. Outlet volume of exhaust gases		B, Exhauster (attach fan cur	ves)		
			ŕ	777	
		in w.g	HP @ _	RPM	
C . Stack height above grade (ft)	D St	ack diameter (ft) or Outlet duct	area (sq. ft.)	E Weather Cap	
Grade elevation (ft)	6.0 fe	et		☐ YES ☒ NO	
Distance from discharge to nearest property line(ft)					
F. Indicate on an attached sheet the location of sampling ports with respect	to exha	ust fan, breeching, etc. Give al	l necessary dimensions.		
To be determined.					
2 POTENTIAL PROCESS EMISSIONS (OUTLET FROM PROCESS, BI	EFORE	ANY CONTROL EQUIPMEN	VT)		
See the attached report sections.					
A. Particulate loading (lbs/hr or gr/DSCF) B. Specific gravity of	f partic	ulate (not bulk density)	C . Attached particle s	size distribution information	
D. Specify gaseous contaminants and concentration					
Contaminant Concentration VOC Contam	inants	Concentration			
(1) SO _x ppm (Vol.)lbs/hr (4)		ppm (Vol.)	lbs/hr		
(2) NO _x ppm (Vol.)lbs/hr (5)		ppm (Vol.)	lbs/hr		
(3) COppm (Vol.)lbs/hr (6) ppm (Vol.)lbs/hr					
E. Does process vent through the control device ? YES NO					
- If YES continue and fill out the appropriate SECTION H - CONTROL I	EQUIPN	IENT			
- If NO skip to SECTION I - MISCELLANEOUS INFORMATION					
F. Can the control equipment be bypassed: (If Yes, explain) YES	S 🛛	NO			
3. ATMOSPHERIC EMISSIONS					
A. Particulate matter emissions (lbs/hr or gr/DSCF)					
See the attached report sections. B. Gaseous contaminant emissions					
		Constanti			
Contaminants Concentration VOC Contaminants					
		ppm (Vol.			
(2) NO _X ppm (Vol.)lbs/h (5)				os/hr	
(3) COppm (Vol.)lbs/h) (6)		ppm (Vol.)lbs/hr		
See the attached report sections.					

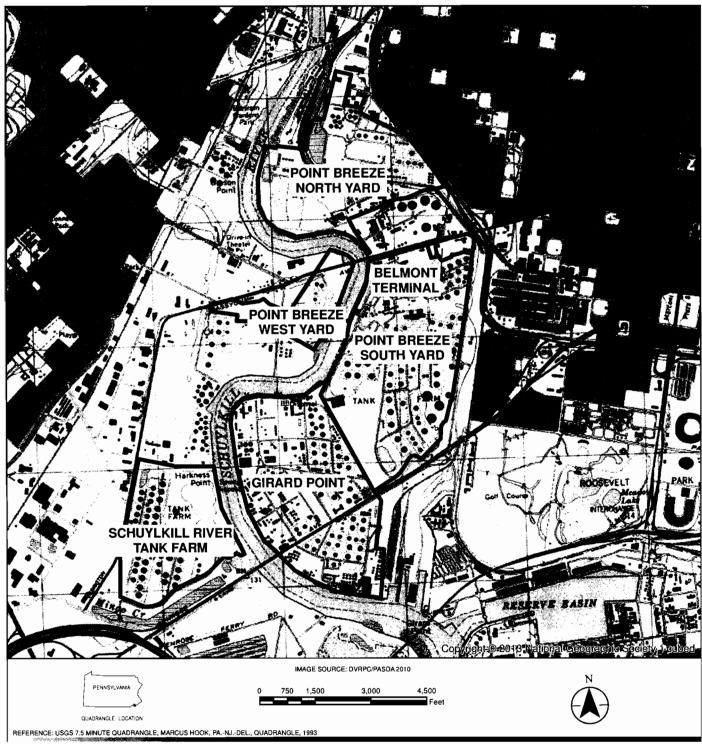
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SECTION H - CONTROL EQUIPMENT, CONTINUED
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Control Equipment Cost:
Direct Cost:
Indirect Cost:
B. Estimated annual operating costs of control equipment only.
13. Describe modifications to control equipment in detail.
Not applicable.
14. Describe in detail the method of dust removal from the air cleaning and methods of controlling fugitive emissions from cust removal, handling and disposal.
Not applicable.
15. Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If so, describe.
Not applicable.
16. Attach manufacturer's performance guarantees and/or warranties for each of the major components of the control system (or complete system).
17. Attach the maintenance schedule for the control equipment and any part of the process equipment that if in disrepair would increase the air contaminant emissions. Periodic maintenance reports are to be submitted to the Department.
Maintenance will be provided as per the manufacturer's recommendations and the Title V Permit.
18. Attach any and all additional information necessary to thoroughly evaluate the control equipment.
See the attached report sections.

- Provide control equipment information on this page if it pertains to this application, otherwise remove this page from the application. If there are more of the same type of control equipment, copy that page and fill in the information as indicated.
- Control equipment can be found from a manufacturer catalogue or vendors.

SECTION I - MISCELLANEOUS INFORMATION					
1. Specify monitoring and recording devices will be used for monitoring and recording of the emission of air contaminants. Provide detailed information to show that the facilities provided are adequate. Include cost and maintenance information.					
☐ Opacity monitoring system ☐ SOx monitoring system ☐ NOx monitoring system ☐ CO monitoring system ☐ CO₂ monitoring system ☐ Oxygen monitoring system ☐ HCL monitoring system ☐ TRS monitoring system ☐ H₂S monitoring system ☐ Temperature monitoring system ☐ Stack flow monitoring system ☐ Other					
If checked, provide manufacturer's name, model no. and pertinent technical specifications.					
No changes proposed from existing monitoring, as outlined in existing Title V Permit. The new Unit 870 H-3 Heater will have a continuous monitor installed to monitor the NOx and oxygen concentration in the heater stack that complies with NSPS Subpart Ja requirements (expected to be similar to Rosemount Model 951C Chemiluminescence).					
2. Attach Air Pollution Episode Strategy (if applicable)					
Not applicable.					
3. If the source is subject to 25 Pa. Code Subchapter E, New Source Review requirements, a. Demonstrate the availability of emission offset (if applicable)					
PES will review the Department's Emission Reduction Credit Registry System to obtain the necessary NO_x and VOC offsets for this project. PES plans to use a portion of the remaining NO_x emission reduction credits (ERCs) generated from the shutdown of certain emissions sources at Marcus Hook as NO_x offsets. The offsets will be surrendered prior to commencement of operation of the affected sources in the manner at which is sought in this plan approval application.					
 Provide an analysis of alternate sites, sizes, production processes and environmental control techniques demonstrating that the benefits of the proposed source outweigh the environmental and social costs. 					
Not applicable.					
See the attached report sections for details.					
4. Attach calculations and any additional information necessary to thoroughly evaluate compliance with all the applicable requirements of Article III of the rules and regulations of Philadelphia Air Management, Pennsylvania Department of Environmental Protection and those requirements promulgated by the Administrator of the United States Environmental Protection Agency pursuant to the provisions of the Clean Air Act.					
See the attached report sections.					
5. List all attachments included in this Application.					
A AMS Plan Approval Application Forms B Site Location Map/Process Flow Diagrams C Back-up Emissions Calculations D Contemporaneous Emissions Tables E Best Available Technology NOx Control Cost Effectiveness Calculations					

Attachment B Site Location Map/Process Flow Diagrams





Stantec Consulting Services Inc.

1060 Andrew Drive, Suite 140 West Chester, Pennsylvania 19380

Tel. 610-840-2500 Fax. 610-840-2501 www.stantec.com

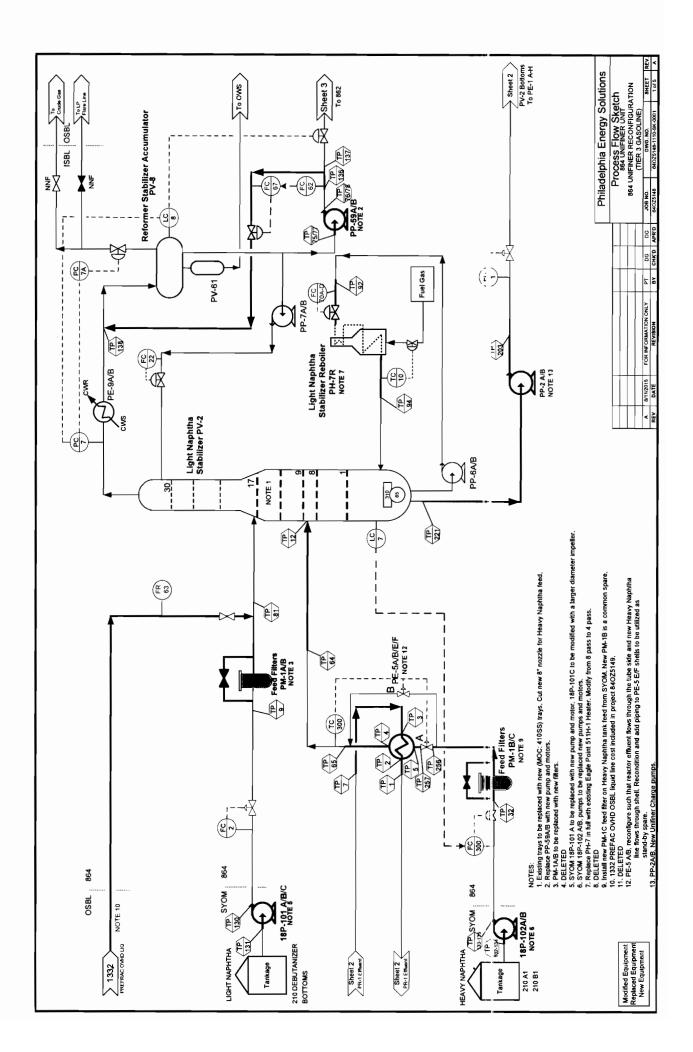
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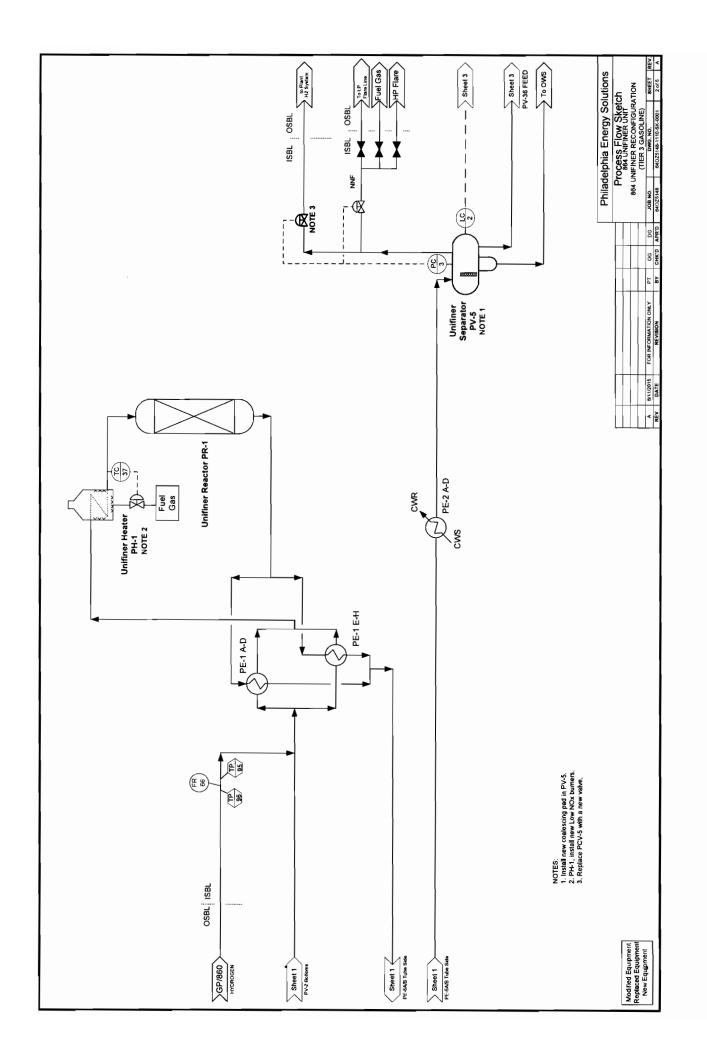
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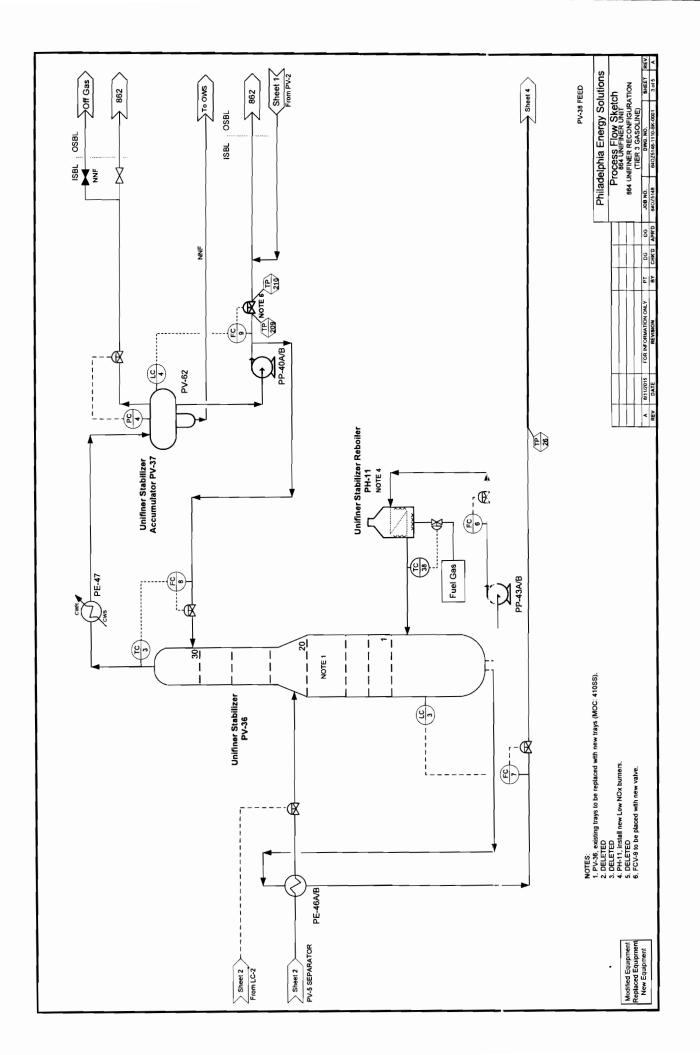
PHILADELPHIA ENERGY SOLUTIONS PHILADELPHIA REFINERY 3144 PASSYUNK AVENUE PHILADELPHIA, PA. 19145

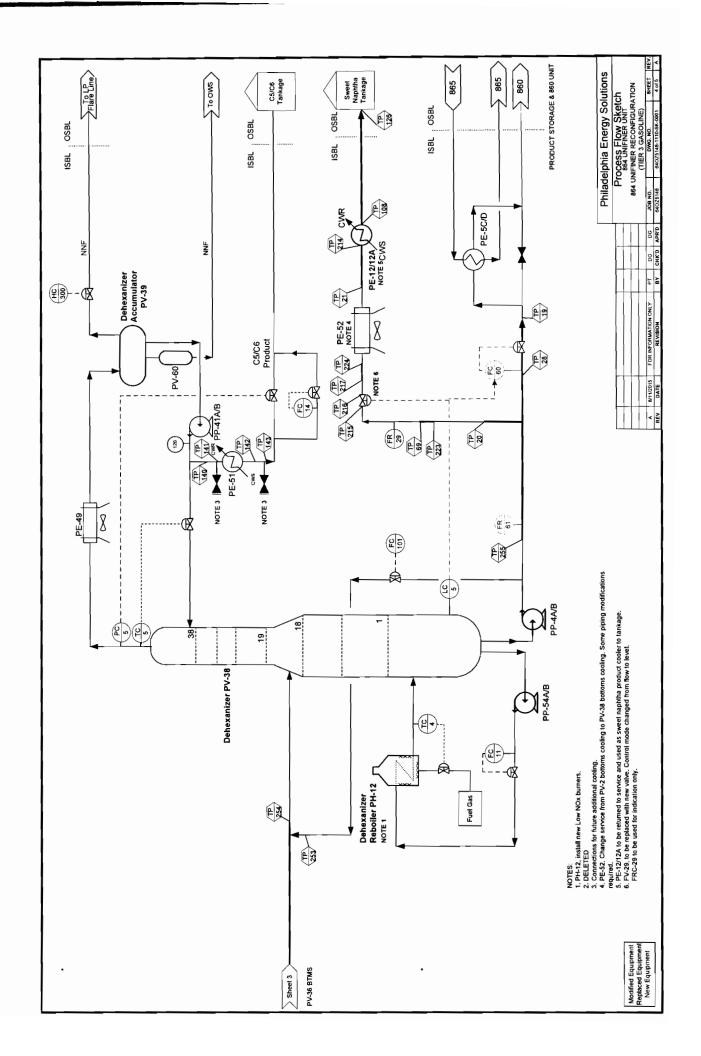
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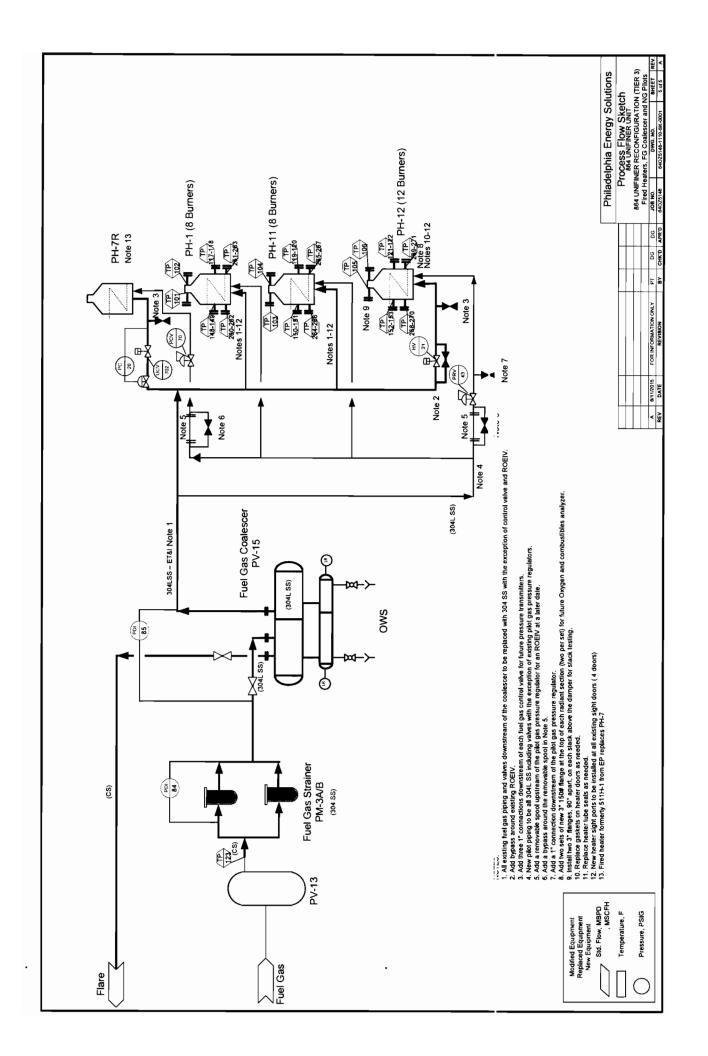
SITE LOCATION MAP

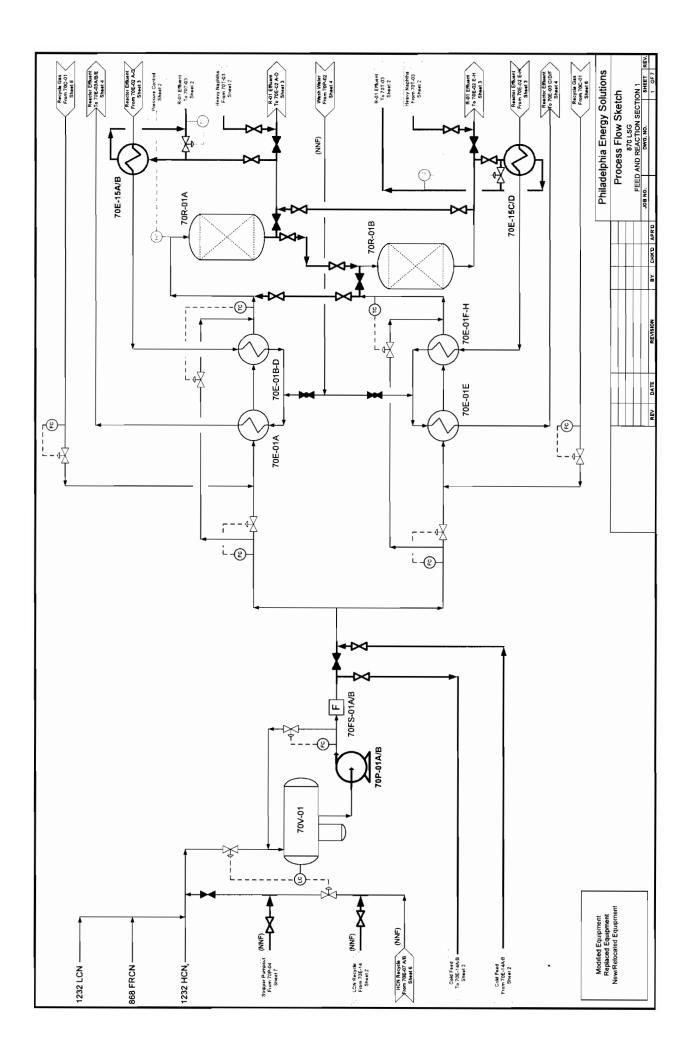


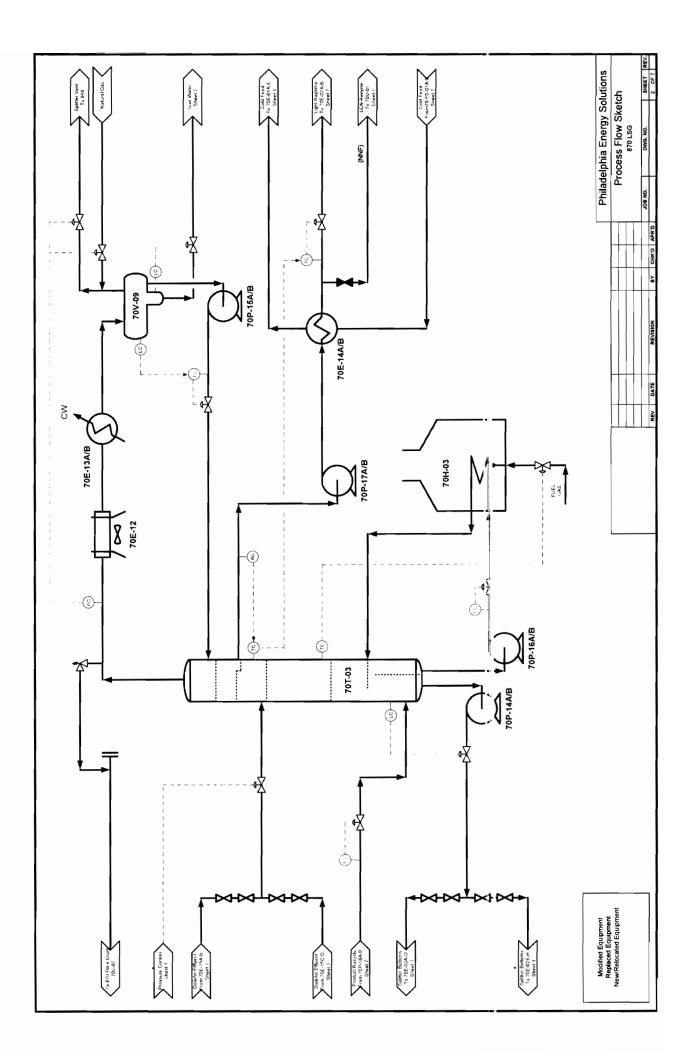


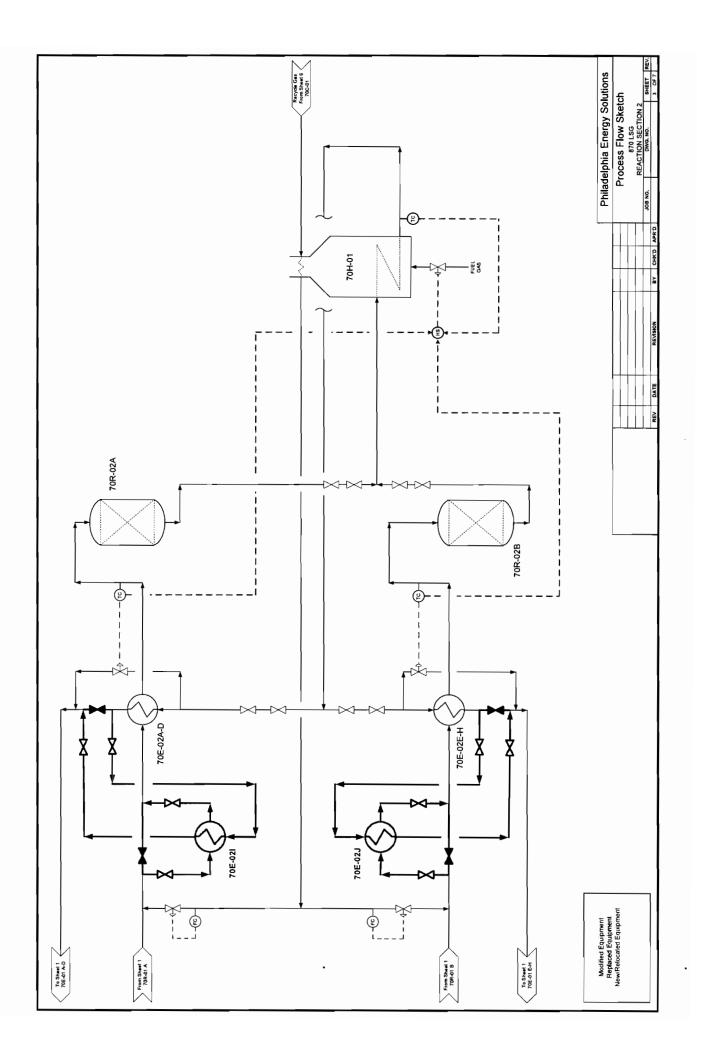


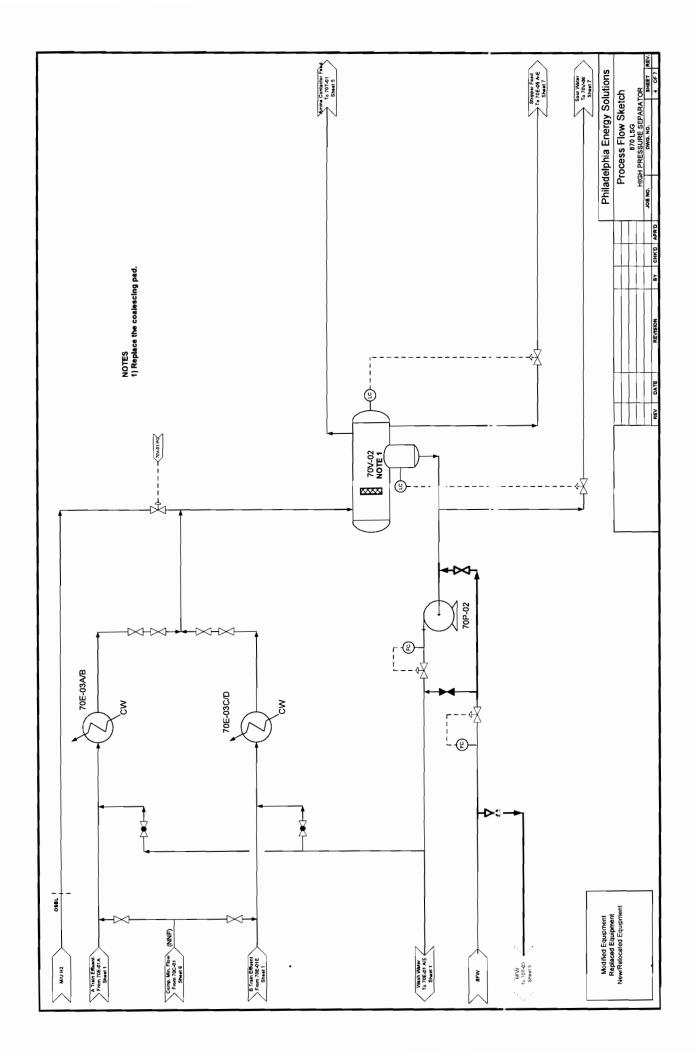


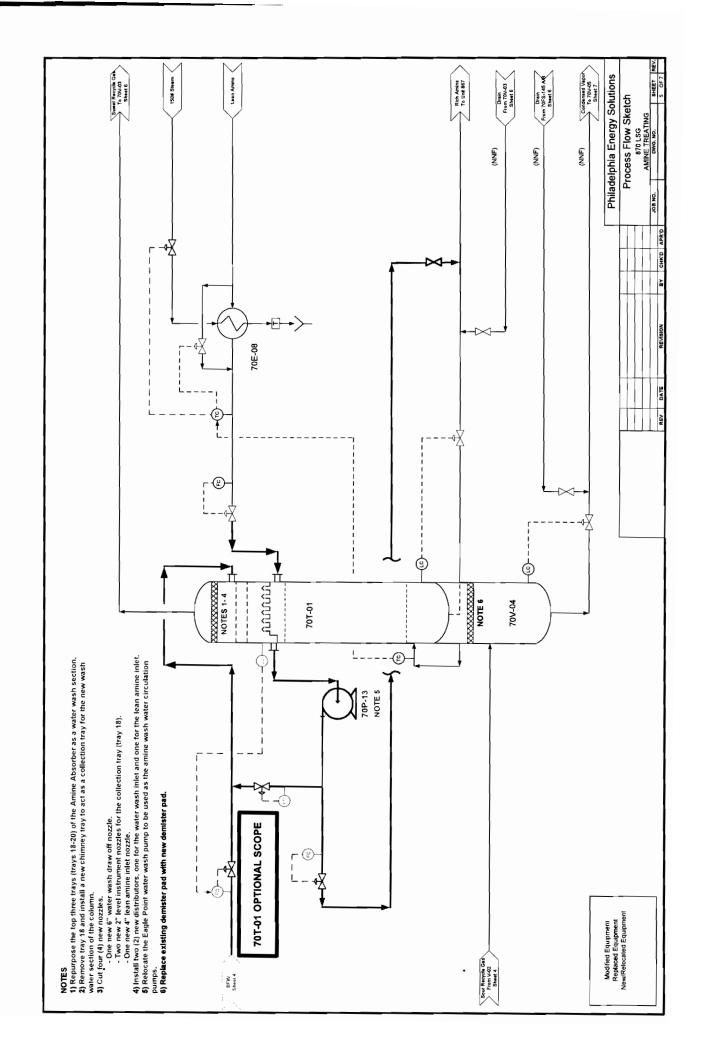


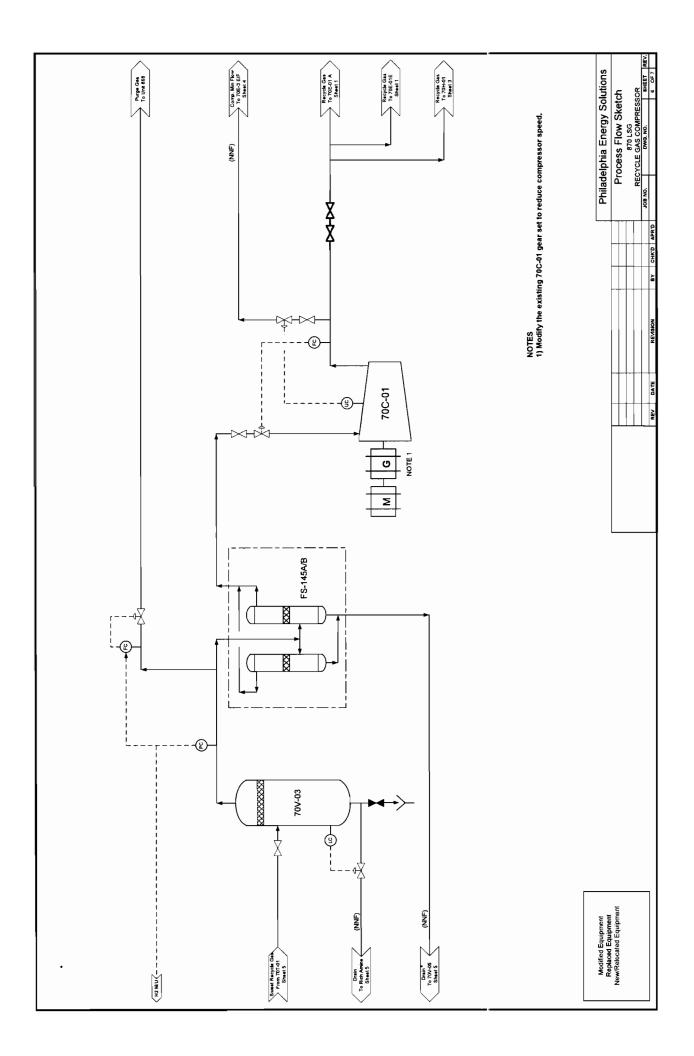


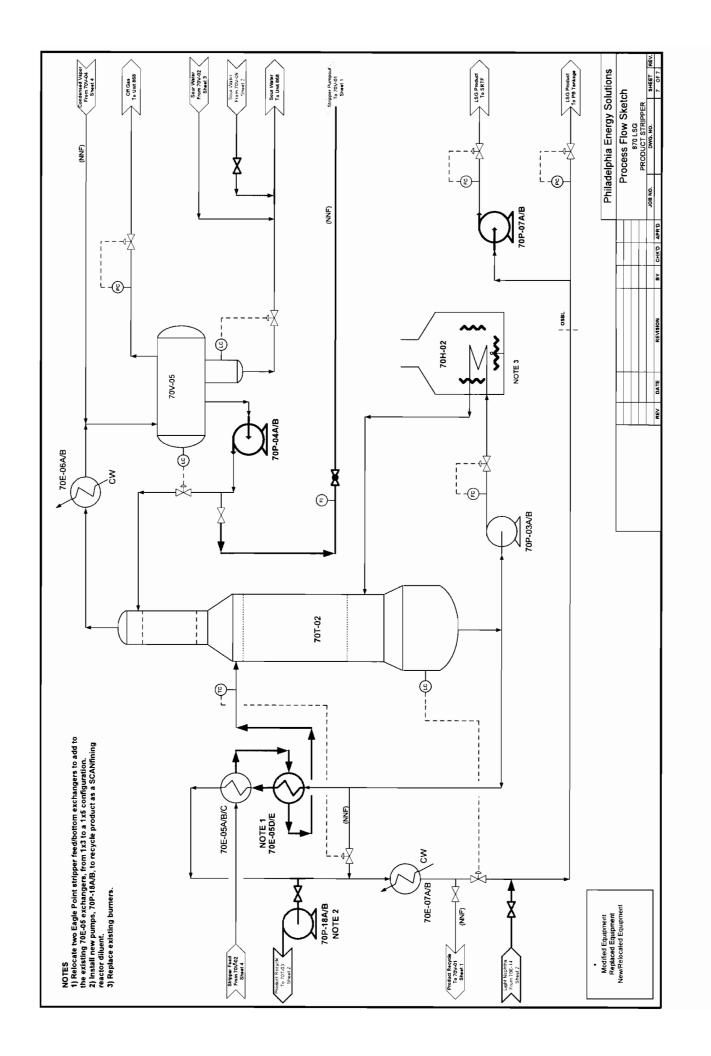


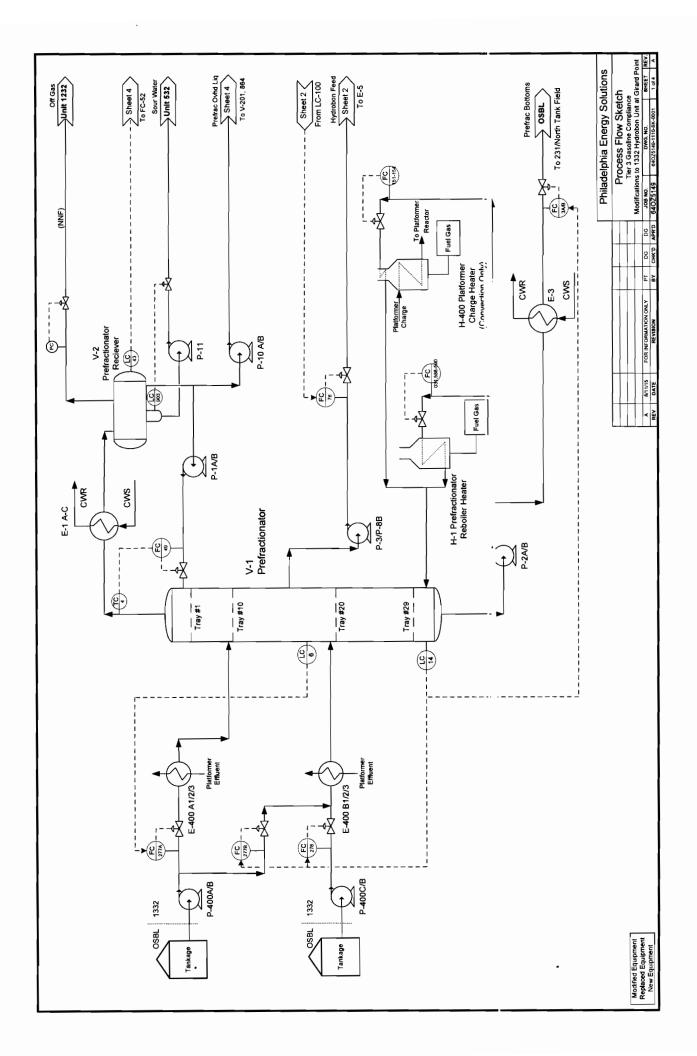


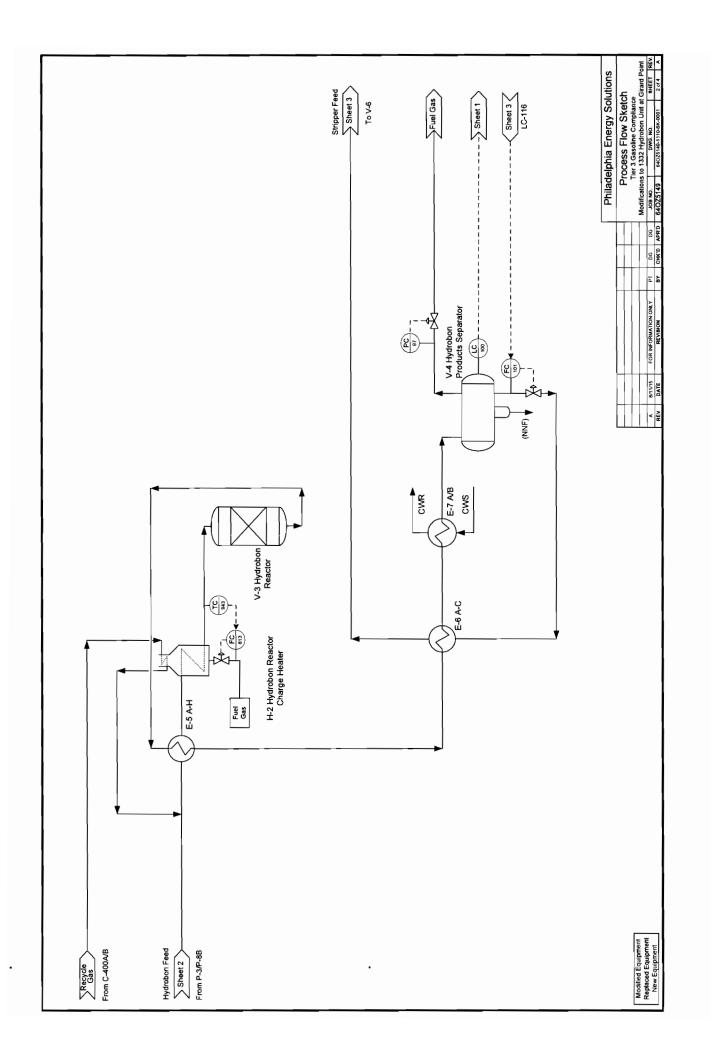


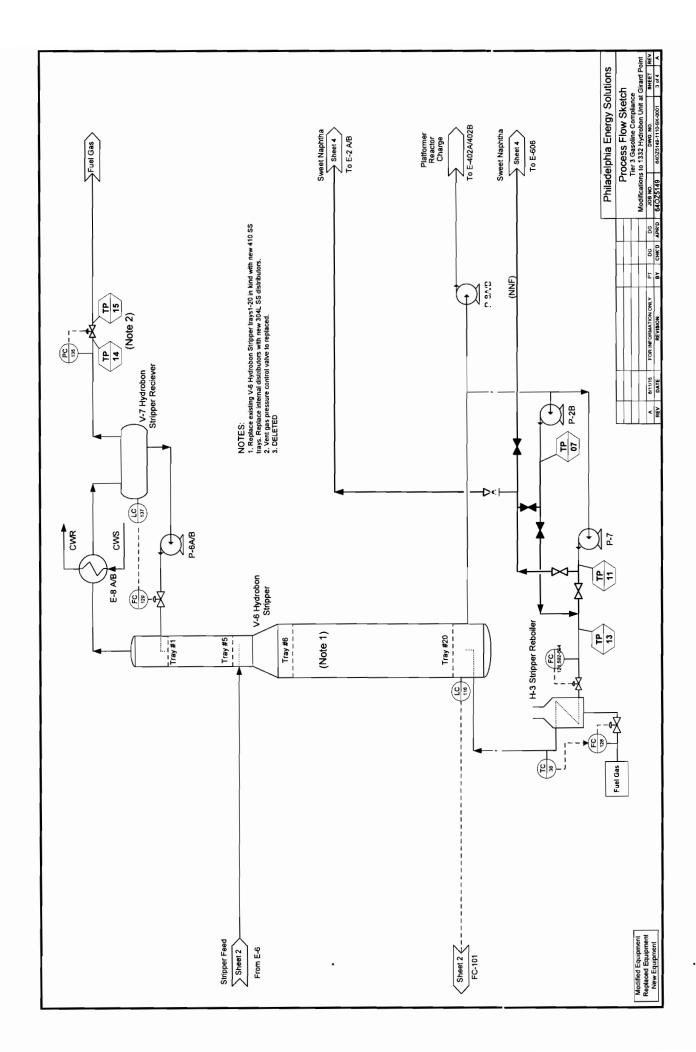


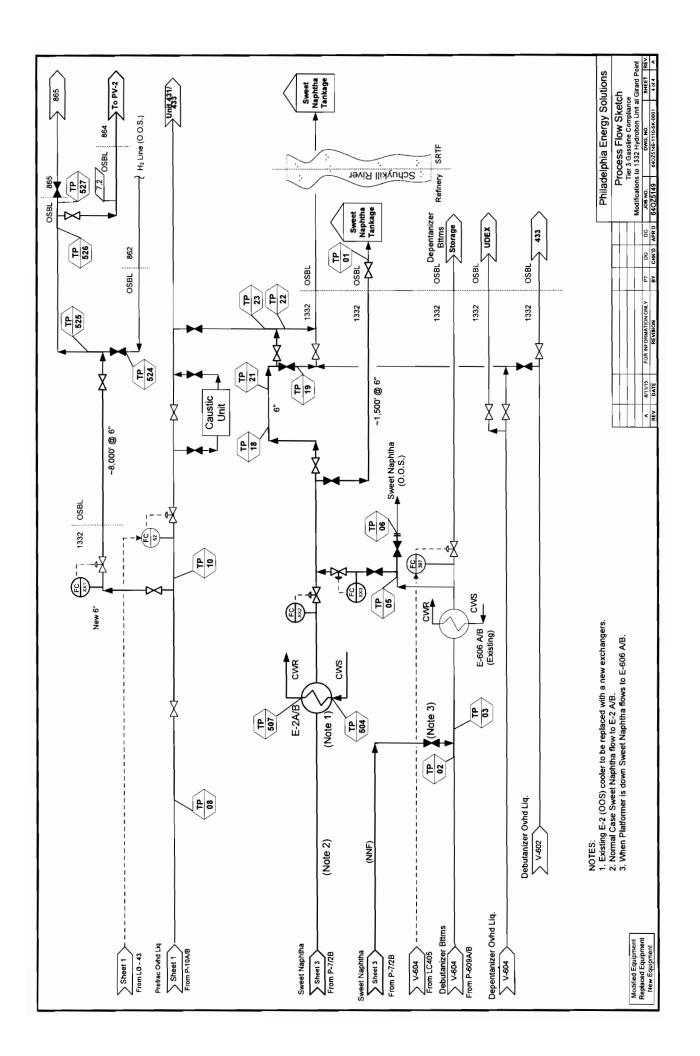












Attachment C Back-up Emissions Calculations

PES Refinery Tier 3 Project Emissions September 2015

Emissions Summary

Source	NO2	NOx	SO_2	00	PM	PM_{10}	PM _{2.5}	NOC	Lead	CO2e
Fired Heaters	34.6	11.2	4.4	66.4	11.9	11.9	6.7	6.5	8.3E-04	200,084
864 PH-1		-2.6	0.5	15.9	1.4	1.4	1.4	1.0	9.4E-05	22,758
864 PH-7		-10.2		:	\$ 1 5			-0.7	1 1 5	1 1
864 PH-7R	6.5	6.5	6.0	9.7	2.3	2.3	0.7	1.6	1.5E-04	35,902
864 PH-11		-6.2	6.4	12.0	1.1	1.1	1.1	8.0	7.1E-05	17,213
864 PH-12		-4.4	9.4	12.1	1.1	1.1	1.1	8.0	7.2E-05	17,341
870 H-1	7.8	7.8	9.0	9.4	1.7	1.7	9.0	0.1	1.3E-04	31,413
870 H-2	2.6	2.6	0.3	0.0	0.2	0.2	0.2	0.1	4.5E-05	10,943
870 H-3	14.5	14.5	1.1	14.5	3.6	3.6	1.1	2.4	2.3E-04	56,417
1332 H-2	1.6	1.6	0.2	0.5	6.4	6.4	6.4	0.3	2.4E-05	6,079
1332 H-3	1.6	1.6	0.1	1.4	0.1	0.1	0.1	0.1	8.1E-06	2,018
Incremental Cooling Water	•	-	-	1	0.2	0.1	0.001	0.1	_	ı
Incremental Sulfur Production	80.0	80.0	0.2	3.3	-	•	-	-	_	•
Fugitive Components	-	-	-	-	-	-	-	0.01	-	-
Total Emissions (TPY)	34.6	11.2	4.7	2.69	12.0	12.0	6.7	6.7	8.3E-04	200,084

PES Refinery Tier 3 Project Emissions September 2015

PSD and NANSR Analysis

					Total Emissions	issions (TPY)					
rarameter	NO2	NOx	SO_2	co	PM	PM_{10}	$PM_{2.5}$	H_2SO_4	Lead	VOC	CO2e
PES Tier 3 Project	34.6	11.2	4.7	69.7	12.0	12.0	6.7	0	8.3E-04	6.7	200,084

		PSD Em	PSD Emissions Analysis (Step 1)	is (Step 1)					
				Pc	Pollutant (TPY)				
rarameter	NO2	so_z	00	Md	PM_{10}	$\mathbf{PM}_{2.5}$	$^{\dagger}OS^{2}H$	Lead	CO_2 e
PES Tier 3 Project	34.6	4.7	2'69	12.0	12.0	6.7	0	8.3E-04	200,084
PSD Significant Level	40	04	100	25	15	10		9.0	22,000
PSD Triggered (Before Netting Analysis)	No	oN	oN	oN	No	No	oN	oN	No

Description	5 calendar	5 calendar
rarameter	year NO _x (TPY)	year VOC (TPY)
PES Tier 3 Project	11.2	6.7
Contemporaneous Increases	12.8	13.2
Net Emissions Increase	24.1	19.8
NANSR Significance Level	25	25
NANSR Review Required	No	oN

Parameter	10 year NO _x (TPY)	10 year NO _x 10 year VOC (TPY)
PES Tier 3 Project	11.2	6.7
Contemporaneous Increases/Decreases	23.4	28.4
Net Emissions Increase	34.6	35.0
NANSR Significance Level	25	
NANSR Review Required	Yes	SəX

Fired Heater Emissions

	Fired Heater	rs		
Unit	Heater	Calculated Firing rate MMBtu/hr	Title V Limits (MMBtu/hr)	Potential Firing Limits (MMBtu/hr)
864	PH-1	47.8	80	74.9
864	PH-7R (former Eagle Point)	56.3	N/A	70
864	PH-11	58.9	74	74
864	PH-12	63.0	85.1	85.1
870	H-1	91.2	97	97
870	H-2	49.9	53	53
870	H-3	103.7	N/A	110
1332	H-2	43.8	60	60
1332	H-3	28.1	43	43

Month		864 (MMBtu/mor	nth)		87	0 (MMBtu/mon	th)	1332 (MMB	tu/ month)
World	PH-1	PH-7R	PH-11	PH-12	H-1	H-2	H-3	H-2	H-3
Jan-12	20,926		26,380	31,175	28,383	25,530		26,602	17,568
Feb-12	18,141		24,371	27,202	26,290	24,007		22,310	16,265
Mar-12	21,611		26,700	28,476	25,106	24,357		26,004	17,277
Apr-12	19,951		25,581	27,441	28,209	24,252		27,503	18,713
May-12	19,318		24,841	26,553	28,312	23,691		25,671	17,60
Jun-12	21,142		27,619	28,387	32,448	26,447		24,763	17,52
Jul-12	19,163		23,954	29,359	23,826	19,764		24,618	17,37
Aug-12	18,625		25,904	28,076	35,139	28,531		21,647	17,32
Sep-12	19,696		27,480	34,568	24,574	21,749		27,716	18,40
Oct-12	21,115		28,627	38,607	29,090	22,822		27,070	18,27
Nov-12	22,585		30,343	41,092	35,113	24,421		26,126	17,37
Dec-12	20,825		28,281	40,118	36,165	27,110		25,102	17,86
Jan-13	21,607		30,179	41,571	36,753	26,428		13,064	9,771
Feb-13	20,012		28,760	37,840	16,174	10,775		0	0
Mar-13	22,542		32,702	40,941	18,803	20,568		15,221	12,00
Apr-13	22,672		31,092	38,163	21,564	26,302		28,797	20,65
May-13	23,866		33,797	38,354	28,667	26,457		26,574	19,69
Jun-13	21,004		28,705	36,446	23,811	26,313		25,199	18,71
Jul-13	24,145		31,918	39,475	18,485	19,887		26,119	18,43
Aug-13	24,032		31,905	39,726	26,289	29,603		26,063	19,75
Sep-13	20,836		30,118	33,383	25,644	25,230		25,502	18,97
Oct-13	22,776		32,317	38,069	24,432	23,324		24,239	20,54
Nov-13	20,979		30,154	38,447	28,360	22,924		26,415	21,79
Dec-13	24,731		30,679	45,798	27,155	20,371		24,422	21,59
Jan-14	24,388		30,029	42,666	24,007	21,724		20,203	18,889
Feb-14	22,235		26,445	41,447	20,598	18,071		14,957	14,71
Mar-14	24,937		32,081	45,672	21,038	17,929		23,728	22,01
Apr-14	26,464		30,784	39,587	25,487	23,007		29,098	20,76
May-14	24,467		24,606	20,810	22,745	24,998		32,199	20,15
Jun-14	31,135		30,000	23,734	18,990	20,856		30,280	17,35
Jul-14	22,060		23,043	22,357	16,713	19,840		30,759	17,693
Aug-14	28,212		28,001	31,399	23,148	22,641		24,476	21,22
Sep-14	25,621		24,245	29,903	23,051	21,695		27,348	20,94
Oct-14	22,747		23,663	29,814	22,571	23,954		34,777	19,239
Nov-14	3,206		1,229	3,326	25,318	22,676		32,129	19,63
Dec-14	18,832		22,640	25,929	29,399	23,450		30,427	19,78
Jan-15	26,295		31,060	31,778	28,834	25,127		26,158	19,29
Feb-15	23,266		27,505	30,556	17,699	15,799		13,223	9,393
Mar-15	31,707		34,715	36,555	23,933	19,042		12,771	11,43
Apr-15	26,508		28,757	33,010	27,043	20,962		23,237	21,53
May-15	27,455		29,409	29,071	27,775	22,671		22,594	20,669
Jun-15	27,758		30,163	28,348	25,331	23,940		25,310	19,080
ne 12 - May 14 Average (MMBtu/hr)	30.5	0.0	40.4	51.3	35.8	31.7	0.0	31,9	24.1
2014 Average HHV (Btu/scf)	1,028	1,029	1,028	1,028	1,028	1,028	1,028	1,066	1,066
seline Emission Factor		864				870		13	22
(lb/MMBtu)	DII 1	_	DIT 11	DII 10	77.1		77.0		
(IU/ MINIDIU)	PH-1	PH-7R	PH-11	PH-12	H-1	H-2	H-3	H-2	H-3

Baseline Emission Factor		864				870		13	32
(lb/MMBtu)	PH-1	PH-7R	PH-11	PH-12	H-1	H-2	H-3	H-2	H-3
NO _x	0.167	0.02	0.145	0.119	0.029	0.028	0.03	0.031	0.0938
SO ₂	0.003	0.003	0.003	0.003	0.002	0.003	0.002	0.004	0.003
СО	0.082	0.032	0.082	0.082	0.0014	0	0.03	0.01	0.0788
PM	0.0074	0.0074	0.0074	0.0074	0.0063	0.0025	0.0074	0.0071	0.0071
PM ₁₀	0.0074	0.0074	0.0074	0.0074	0.0063	0.0025	0.0074	0.0071	0.0071
PM _{2.5}	0.0074	0.0023	0.0074	0.0074	0.0023	0.0023	0.0023	0.0071	0.0071
VOC	0.0053	0.0053	0.0053	0.0053	0.0004	0.0009	0.0050	0.0052	0.0052
Lead	4.9E-07	4.7E-07	4.7E-07						
CO ₂ e	117.1	117.1	117.1	117.1	117.1	117.1	117.1	117.1	117.1

Fired Heater Emissions

Emissions Increases (lb/hr)		864				8'71		13	32
Emissions increases (10/ nr)	PH-1	PH-7R	PH-11	PH-12	H-1	H	H-3	H-2	H-3
NO _x	2.89	1.48	2.68	1.39	1.61	0.5	3.30	0.37	0.37
SO ₂	0.05	0.20	0.05	0.03	0.13	0.5	0.25	0.04	0.01
CO	1.41	2.22	1.51	0.96	0.08	0. %	3.30	0.12	0.31
PM	0.13	0.52	0.14	0.09	0.35	0. 5	0.81	0.08	0.03
PM ₁₀	0.13	0.52	0.14	0.09	0.35	0.):	0.81	0.08	0.03
PM _{2.5}	0.13	0.16	0.14	0.09	0.13	0.0	0.25	0.08	0.03
VOC	0.09	0.37	0.10	0.06	0.02	0.5.	0.55	0.06	0.02
Lead	8.4E-06	3.4E-05	9.0E-06	5.7E-06	2.7E-05	8.91:- 16	5.3E-05	5.6E-06	1.8E-06
CO ₂ e	2,025	8,197	2,162	1,370	6,499	2,14	12,881	1,388	461
Incremental Emissions		864				8.7		12	32
Increases (TPY)	PH-1	PH-7R	PH-11	PH-12	H-1	T #:	H-3	H-2	H-3
NO _v	12.65		11.73	6.10	7.05	2.3		1.61	1.62
SO ₂	0,21		0.23	0.14	0.56	0.1		0.19	0.05
CO	6.19		6.61	4.18	0.33	0.3		0.52	1.36
PM	0.56		0.60	0.38	1.52	0.5		0.32	0.12
PM ₁₀	0.56		0.60	0.38	1.52	0.5		0.37	0.12
PM _{2.5}	0.56		0.60	0.38	0.55	0. 8		0.37	0.12
VOC	0.41		0.43	0.27	0.10	0.05		0.27	0.09
Lead	3.7E-05		3.9E-05	2.5E-05	1.2E-04	3.91 - ₹ 5		2.4E-05	8.1E-06
CO ₂ e	8.869		9.471	5,999	28,463	9,37		6,079	2,018
								-,	
Potential Emissions		864				870		13	
Increases (TPY)	PH-1	PH-7R	PH-11	PH-12	H-1	H-2	H-3	H-2	H-3
NO _x	32.46	6.48	21.32	17.62	7.78	2.62	14.45	3.82	7.76
SO ₂	0.55	0.87	0.41	0.40	0.62	0.15	1.11	0.45	0.26
СО	15.87	9.72	12.01	12.10	0.37	0.00	14.45	1.23	6.52
PM	1.44	2.27	1.09	1.09	1.68	0.74	3.56	0.88	0.59
PM ₁₀	1.44	2.27	1.09	1.09	1.68	0.74	3.56	0.88	0.59
PM _{2.5}	1.44	0.70	1.09	1.09	0.61	0.73	1.10	0.88	0.59
VOC	1.04	1.62	0.79	0.79	0.10	0.(3	2.41	0.64	0.43
Lead	9.4E-05	1.5E-04	7.1E-05	7.2E-05	1.3E-04	4.5E - 5	2.3E-04	5.8E-05	3.9E-05
CO ₂ e	22,758	35,902	17,213	17,341	31,413	10,54	56,417	14,413	9,683

	Baseline Emissions		
Actual Emissions (TPY)	864	864	864
Actual Emissions (111)	PH-1	PH-11	PH-12
Average MMBtu/hr	30.5	40.4	51.3
NO _x	22.33	25.68	26.73
SO ₂	0.38	0.49	0.61
СО	10.92	14.47	18.35
PM	0.99	1.31	1.66
PM ₁₀	0.99	1.31	1.66
PM _{2.5}	0.99	1.31	1.66
VOC	0.72	0.95	1.20
Lead	6.5E-05	8.6E-05	1.1E-04
CO ₂ e	15,657	20,740	26,306

	LNB Modified Heat	er	
Fortune Batantial (TD)()	864	864	864
Future Potential (TPY)	PH-1	PH-11	PH-12
MMBtu/hr	74.9	74	85.1
NO _x	19.68	19.45	22.36
SO ₂	0.92	0.91	1.01
co	26.79	26.47	30.44
PM	2,42	2.40	2.75
PM ₁₀	2.42	2.40	2.75
PM _{2.5}	2.42	2.40	2.75
VOC	1.75	1.73	1.99
Lead	1.6E-04	1.6E-04	1.8E-04
CO₂e	38,415	37,953	43,646
LNB NO _x Emission Rate	0.06	0.06	0.06

	LNB Modified Heat	er	
Emissions Inspector (TDV)	864	864	864
Emissions Increases (TPY)	PH-1	PH-11	PH-12
MMBtu/hr increase	44.4	33.6	33.8
NO _x	-2.65	-6.24	-4.37
SO ₂	0.55	0.41	0.40
СО	15.87	12.01	12.10
PM	1.44	1.09	1.09
PM ₁₀	1.44	1.09	1.09
PM _{2.5}	1.44	1.09	1.09
VOC	1.04	0.79	0.79
• Lead	9.4E-05	7.1E-05	7.2E-05
CO ₂ e	22,758	17,213	17,341

(lb/MMBtu)

PES Refinery Tier 3 Project Emissions September 2015

864 PH-7 Shutdown Summary

5.9E-05	5.6E-05	5.9E-05	4.9E-05	6.4E-05	5.5E-05	Lead
13,511	13,093	13,374	11,227	14,959	11,790	CO_2e
0.65	0.62	0.65	0.53	0.71	09:0	VOC
0.90	0.85	06:0	0.73	26.0	0.83	PM
9.93	9.42	6.97	8.06	10.77	9.16	ĊO
0.33	0.33	0.32	0.29	0.36	0.28	SO_2
10.15	11.29	60.6	98.6	12.72	5.47	NOx
June '12 - May '14	2013/2014	$2012/20\overline{13}$	2014	2013	2012	Pollutant

Tier 3 Project Emissions September 2015

PES Refinery

Unit 864 PH-7R Heater (Replacement from Eagle Point Refinery)

	Btu			4		3	2	
	lb/MMBtu	0.032	0.02	0.0074	0.003	0.0053	4.9E-07	1171
	TPY	2.6	6.5	2.3	6.0	1.6	1.5E-04	35 902
70.0	lb/hr	2.22	1.48	0.52	0.20	0.37	3.4E-05	8 197
Fired Duty (MMBtu/hr)	Pollutant	CO	NOx	$\overline{{ m PM}_{10}}$	SO_2	VOC	Lead	CO.e

Tier 3 Project Emissions September 2015 PES Refinery

Unit 870 H-3 Heater (New Heater)

	_							_
	lb/MMBtu	0:030	0.03	0.0074	0.002	0.0050	4.9E-07	117.1
	TPY	14.5	14.5	3.6	1.1	2.4	2.3E-04	56,417
110.0	lb/hr	3.3	3.3	0.81	0.25	0.55	5.3E-05	12,881
Fired Duty (MMBtu/hr)	Pollutant	CO	NO _x	PM_{10}	SO ₂	VOC	Lead	CO,e

PES Refinery Tier 3 Project Emissions September 2015

Fired Heater SO, Emissions

2013 Firing	ring	2013 SO ₂ Emissions	2014 Firing	2014 SO ₂	24 Month Average
(MMBtu)		(tons)	(MMBtu)	Emissions (tons)	(10 SO ₂ / MIMBtu)
269,202		0.37	274,304	0.39	0.0028
372,326		0.52	296,766	0.42	0.0028
468,212		0.64	356,643	0.48	0.0027
296,138 0	0	0.28	273,065	0.37	0.0023
278,182 0	0	0.35	260,841	0.37	0.0027
261,616		0.41	330,380	89.0	0.0037
201,939)	0.28	232,411	0.41	0.0032
202,370		0.29	193,024	0.32	0.0031
295,751		0.42	337,219	0.59	0.0032

PES Refinery Tier 3 Project Emissions September 2015

Incremental Cooling Tower Emissions

Parameter	Value
Unit Name	864 Cooling Tower
Number of Units	1
Design Water Flow Rate (gpm)	600
Cooling Tower Drift Rate (% of circulating water)	0.005
Total Dissolved Solids (ppm)	600
Cycles of Concentration Ratio (tower/makeup water)	4
VOC EF (lb/MMgal)	0.7
PM ₁₀ Fraction	0.8843
PM _{2.5} Fraction	0.0047

Parameter	PM ¹	PM ₁₀ ²	PM _{2.5} ²	VOC
Hourly (lb/hr)	0.04	0.03	0.0002	0.03
Daily (lb/day)	0.9	0.8	0.004	0.60
Annual (TPY)	0.2	0.1	0.001	0.11

¹ PM calculated based on flow rate, drift rate, and total dissolved solids.

Factors:

60 min/hr 8.345 water density (CWS) 8760 hr/yr 2000 lb/ton

Example from Reisman/Frisbie Paper

Example from Reismany Prisole P			Particle Mass		Solid Particle	
	Droplet	Droplet Mass	(Solids)	Solid Particle	Diameter	EPRI % Mass
EPRI Droplet Diameter (µm)	Volume (μm³)	(μg)	(μg)	Volume (μm³)	(μm)	Smaller
10	524	5.24E-04	3.14E-07	0.14	0.649	0.000
20	4189	4.19E-03	2.51E-06	1.14	1.297	0.196
30	14137	1.41E-02	8.49E-06	3.86	1.946	0.226
40	33510	3.35E-02	2.01E-05	9.14	2.595	0.514
50	65450	6.55E-02	3.93E-05	17.86	3.243	1.816
60	113097	1.13E-01	6.79E-05	30.86	3.892	5.702
70	179594	1.80E-01	1.08E-04	49.01	4.540	21.348
90	381704	3.82E-01	2.29E-04	104.16	5.838	49.812
110	696910	6.97E-01	4.18E-04	190.18	7.135	70.509
130	1150347	1.15E+00	6.91E-04	313.92	8.432	82.023
150	1767146	1.77E+00	1.06E-03	482.24	9.729	88.012
180	3053628	3.06E+00	1.83E-03	833.31	11.675	91.032
210	4849048	4.85E+00	2.91E-03	1323.26	13.621	92.468
240	7238229	7.24E+00	4.35E-03	1975.25	15.567	94.091
270	10305995	1.03E+01	6.19E-03	2812.41	17.513	94.689
300	14137167	1.41E+01	8.49E-03	3857.90	19.459	96.288
350	22449298	2.25E+01	1.35E-02	6126.21	22.702	97.011
400	33510322	3.35E+01	2.01E-02	9144.66	25.945	98.340
450	47712938	4.77E+01	2.86E-02	13020.42	29.188	99.071
500	65449847	6.55E+01	3.93E-02	17860.66	32.431	99.071
600	113097336	1.13E+02	6.79E-02	30863.22	38.918	100.000

 $^{^{\}rm 2}$ Reisman, J. and Frisbie, G., "Calculating Realistic PM10 Emissions From Cooling Towers."

PES Refinery Tier 3 Project Emissions September 2015

Incremental Sulfur Production Emissions

From 867 (2013)	Total Sulfur (Tons)
Jan-13	697.7
Feb-13	417.3
Mar-13	490.1
Apr-13	635.8
May-13	720.5
Jun-13	832.8
Jul-13	949.0
Aug-13	950.3
Sep-13	843.6
Oct-13	818.0
Nov-13	651.1
Dec-13	627.5
Total	8,633.7

2013 Total Err issions	5
TOTAL SRU NO _x (ton)	4.4
TOTAL SRU CO (ton)	172.2
TOTAL SRU SO ₂ (ton)	11.5

Additional Sulfur Production from 864/870

Total

894.6

lb/day =

326,518 lb/yr =

163.3 TFY

D	Total Sulfur			SO ₂
Parameter	(tons)	NO_x (TPY)	CO (TPY)	(TPY)
Future Total (TPY)	8,797.0	4.5	175.5	11.7
Increase (TPY)	163.3	0.1	3.3	0.2

PES Refinery Tier 3 Project Emissions

September 2015

Fugitive Emission Estimates

34; u11 028/878		Additiona	Additional Components	
STUC 0/0/200	Valves	Flanges	$\operatorname{sdun}_{\operatorname{\mathbf{d}}}$	Connectors
Process Modifications*	125	250	13	0
Default-zero Emission Rate	7.8E-06	3.1E-07	2.4E-05	7.5E-06
(kg/ nr/ source)				
(lb/yr/source)	1.5E-01	6.0E-03	4.6E-01	1.5E-01

Total VOC Emissions (lb/yr)	18.88	1.50	6.04	0
Total VOC Emissions (lb/yr)			26.42	
Total VOC Emissions (lb/hr)			0.003	
Total VOC Emissions (TPY)			0.013	

^{*}All component counts are estimated at 115% to allow for final design flexibility

^{**} EPA 1995 Protocol for Equipment Leak Emission Estimates, Table 2-12

Attachment D Contemporaneous Emissions Tables

			Effective Date of			PSD N	PSD Net Emission Change, Ton/Yr	nge, Ton/Yr		
Facility	Fermit No.	Activity	Change ¹	NO2	SO_2	PM/PM ₁₀ /PM ₂₅	co	H ₂ SO ₄	Lead	CO ₂ e
Gir. Pt./Pt. Br.	RFD	3-Unit Train - Crude Transfer Pipeline	1/18/2013	0.00	0.00	0.00	Modeled	0.00	0.00E+00	0
Point Breeze	13001	Tank P-590 (PB 843) Reactivation ²	1/22/2013	0.27	0.18	0.05	Modeled ³	0.00	0.00E+00	0
Gir. Pt./Pt. Br.	12270	Butane Truck Unloading at SRTF	3/5/2013	60:0	0.00	0.00	Modeled ³	0.00	0.00E+00	0
Gir. Pt./Pt. Br.	13020	14-Unit Train - Crude Transfer Pipeline	4/8/2013	0.00	0.00	0.00	Modeled ³	0.00	0.00E+00	0
Point Breeze	RFD	210 Light-Ends Improvement Project	8/21/2013	0.00	0.00	0.00	0.00	0.00	0.00E+00	0
Girard Point	RFD	Butane Logistics Project	1/13/2014	0.00	0.00	0.00	0.00	0.00	0.00E+00	0
Gir. Pt./Pt. Br.	12195	Heater Firing Rate Increase (7-Heater)	2/19/2014	237.42	12.57	20.31	Modeled ³	0.00	1.77E-03	261,670
Point Breeze	RFD	210 VTB Cooling	3/21/2014	0.00	0.00	0.00	0.00	0.00	0.00E+00	0
Girard Point	14045	Butane Railcar Unloading	4/08/2014	0.56	0.04	0.11	1.31	0.00	0.00E+00	1,239
Point Breeze	13260	South Yard South Flare	7/18/2014	1.44	0.03	90:0	6.92	0.00	0.00E+00	618
Point Breeze	RFD	868 TCSS Distillate Recovery	6/9/2014	1.00	80.0	0.20	2.07	0.00	0.00E+00	0
Girard Point	CLEN	1232 Distillate Recovery	7/25/2014	2.08	0.03	0.39	5.60	0.00	0.00E+00	0
Point Breeze	G£X	PB 210 V2 Stripper	7/25/2014	0.48	-6.85	-3.35	1.63	0.00	0.00E+00	0
Girard Point	14219-14220	Butane Terminal Firewater Pumps	8/11/2014	0.00	0.00	0.00	0.00	0.00	0.00E+00	0
Point Breeze	14237	Tank PB 36 (P-010) Gasoline Storage	8/29/2014	0.00	0.00	0.00	0.00	0.00	0.00E+00	0
Gir. Pt./Pt. Br.	14149	Boiler 45	9/2/2014	5.06	15.15	6.13	5.69	2.32	7.61E-04	182,774
Girard Point	CLEN	1332 C-703 Steam Heat Exchanger	10/9/2014	0.21	0.00	0.01	0.13	0	0	0
Point Breeze	RFD	868 LCO Recovery Improvements	10/16/2014	0.75	0.14	0.16	2.65	0	0	0
Point Breeze	RFD	210C VTB Direct to 868	11/17/2014	0.21	0.34	0.19	0.85	0	0	0
Point Breeze	CLEN	137 Depropanizer Feed	10/16/2014	0.00	0.00	0.00	0.00	0	0	0
Girard Point	G£X	433 Propane Processing Improvements	10/28/2014	1.00	0.07	0.20	2.22	0	0	0
Point Breeze	GED	210 Debutanizer Cooling	Pending	0.00	0.00	0.00	0.00	0	0	0
Girard Point	RFD	1232 Absorber/ Stripper Tower	12/8/2014	0.00	0.00	0.00	0.00	0	0	0
Point Breeze	14368	Tank PB-848 Crude Storage	12/15/2014	0.00	0.00	0.00	0.00	0	0	0
Point Breeze	14369	Tank PB-844 Crude Storage	12/15/2014	0.00	0.00	0.00	0.00	0	0	0
Girard Point	RFD	GP 433 Emergency Relief	12/2/2014	0.00	0.00	0.00	0.00	0	0	0
Point Breeze	RFD	HDS Field Charge Pump	12/16/2014	90.0	0.20	0.13	2.26	0	0	0
Girard Point	RFD	Crude Off-loading Flexibility	Pending	0.00	0.00	0.00	0.00	0	0	0
Point Breeze	RFD	Tank PB-880 Crude Storage	Pending	0.00	0.00	0.00	0.00	0	0	0
Point Breeze	RFD	Tank PB-850 Crude Storage	Pending	0.00	0.00	0.00	0.00	0	0	0
Point Breeze	Application	Unit 864 PH-1, Unit 864 PH-11, Unit 864 PH-12 Heater Burner Replacements	Application	-11.91	00:00	00.00	0.00	0	0	0
Point Breeze	Application	Replacement of 864 PH-7	Application	-11.29	-0.33	-0.85	-9.42	0	0	-13,093
	5-year in	5-year increases and decreases from 1st Quarter 2015		227.42	21.64	23.74	21.91	2.32	2.53E-03	433,208

Notes:

1 of 4

¹ The Effective Date of Change for emissions increases is considered the date of permit issuance and for emissions reductions it is the date of source shutdown.

2 Tank P-590 (PB 843) includes emissions from No. 3 Boiler House that were already permitted in No. 3 Boiler House NOx Reduction Project in 2008.

3 Plan Approval 12195 triggered PSD Modeling for CO, which showed no CO concentration from project and contemporaneous projects that were above the CO SIL. Therefore, all increases from 9/9/2008 through 9/6/13 (date of application) are excluded from future project netting.

25 Pa Code 127.203(b)(1)(i) 5 Calendar Year Increases

		4 74 74 7			
Facility	Permit No.	Activity	Effective Date of	NANSR Net Emission Change, Ton/Yr	t Emission Ton/Yr
			Change	VOC	NOx
Gir. Pt./Pt. Br.	RFD	3-Unit Train - Crude Transfer Pipeline	1/18/2013	Offset ²	0.00
Point Breeze	13001	Tank P-590 (PB 843) Reactivation ³	1/22/2013	Offset ²	Offset ²
Gir. Pt./Pt. Br.	12270	Butane Truck Unloading at SRTF	3/5/2013	Offset ²	Offset ²
Gir. Pt./Pt. Br.	13020	14-Unit Train - Crude Transfer Pipeline	4/8/2013	Offset ²	00.0
Point Breeze	RFD	210 Light-Ends Improvement Project	8/21/2013	0.01	0.00
Girard Point	RFD	Butane Logistics Project	1/13/2014	0.0005	0.00
Gir. Pt./Pt. Br.	12195	Heater Firing Rate Increase (7-Heater)	2/19/2014	Offset ²	Offset ²
Point Breeze	777	210 VTB Cooling	3/21/2014	0.002	0.00
Girard Point	14045	Butane Railcar Unloading	4/08/2014	2.70	0.56
Point Breeze	13260	South Yard South Flare	7/18/2014	2.42	1.44
Point Breeze	RFD	868 TCSS Distillate Recovery	6/9/2014	0.15	1.00
Girard Point	RFD	1232 Distillate Recovery	7/25/2014	0.30	2.08
Point Breeze	RFD	PB 210 V2 Stripper	7/25/2014	0.15	0.48
Girard Point	14219-14220	Butane Terminal Firewater Pumps	8/11/2014	0.00	0.00
Gir. Pt./Pt. Br.	14149	Boiler 45	9/2/2014	1.45	5.06
Girard Point	RFD	1332 C-703 Steam Heat Exchanger	10/09/2014	0.01	0.21
Point Breeze	RFD	868 LCO Recovery Improvements	10/16/2014	0.11	0.75
Point Breeze	RFD	210C VTB Direct to 868	11/17/2014	0.03	0.21
Point Breeze	RFD	137 Depropanizer Feed	10/16/2014	0.00	0.00
Girard Point	RFD	433 Propane Processing Improvements	10/28/2014	0.16	1.00
Point Breeze	RFD	210 Debutanizer Cooling	Pending	0.00	0.00
Girard Point	RFD	1232 Absorber/ Stripper Tower	12/8/2014	0.03	0.00
Point Breeze	14368	Tank PB-848 Crude Storage	12/15/2014	1.01	0.00
Point Breeze	14369	Tank PB-844 Crude Storage	12/15/2014	1.09	0.00
Girard Point	RFD	GP 433 Emergency Relief	12/2/2014	0.00	0.00
Point Breeze	RFD	HDS Field Charge Pump	12/16/2014	0.09	0.06
Girard Point	RFD	Crude Off-loading Flexibility	1/8/2015	0.00	0.00
SRTF	RFD	Butane Blending at SRTF	3/2/2015	0.00	0.00
Point Breeze	RFD	Tank PB-880 Crude Storage	Pending	1.24	0.00
Point Breeze	RFD	Tank PB-850 Crude Storage	Pending	1.24	0.00
SRTF	Pending	Butane Compressor	Pending	0.01	0.00
Point Breeze	14237	Tank PB 36 (P-010) Gasoline Storage	Pending	0.97	0.00
	5-calend	5-calendar year increases from 1st Quarter 2015 ^{4,5}		13.17	12.84
17-1					

Notes:

- 1 The Effective Date of Change for emissions increases is considered the date of permit issuance and for emissions reductions it is the date of source shutdown.

 2 Plan Approval 12195 triggered NSR for VOC & NO_r. All increases from calendar years 2009 through 9/6/13 (date of
- application) were offset.
- 3 Tank P-590 (PB 843) includes emissions from steam from No. 3 Boiler House that were already permitted in No. 3 Boiler House NO_x Reduction Project in 2008.
- 4 NSR contemporaneous period for VOC and NO₂ is 5 calendar years (the year of modification plus back 4 more years). 5 Consent Decree emissions credits from the shutdown of the Marcus Hook 10-4 FCC and LSG units are not available except in certain situations as described in the Consent Decree.

25 Pa Code 127.203(b)(1)(ii) 10 Year Increases/Decreases

		5 Pa Code 127.203(b)(1)(ii) 10 Year Increas	Effective Date of	NANSR Ne	
Facility	Permit No.	Activity Change ¹ 1232 Flue Gas Treating & Expansion 2/28/2006		Change,	
Gir. Pt./Pt. Br.	04322	1232 Flue Cas Treating & Evpansion	2/28/2006	0.00	NO _x 0.00
Point Breeze	05219	866 Unit Modification for ULSD mode	3/7/2006	0.00	0.00
Girard Point	NA NA	Demin, valves and flanges at Units 433/869	2006	0.00	0.00
Girard Point	06050	433 HFAU Process Improvement Project	12/4/2006	0.00	0.00
Girard Point	07026	231 Imported Jet Project	6/13/2007	0.00	0.00
Gir. Pt./Pt. Br.	06144	859 ULSD Project ³	1/29/2008	0.00	0.00
Gir. Pt./Pt. Br.	08080	No. 3 Boiler House NO _x Reduction	9/9/2008	12.52	0.00
Girard Point	RFD	Unit 433 KOH Treater Lines	10/23/2008	0.01	0.19
Point Breeze	RFD	Unit 866 Stripper Valve	12/22/2008	0.30	0.06
Point Breeze	08255	Unit 865 Improvement Project	2/23/2009	0.97	9.42
Girard Point	09022	Unit 137 RFG Changes	3/3/2009	0.02	0.00
Girard Point	09116	Unit 433 ASO to Unit 137 Desalter	6/5/2009	0.02	0.00
Girard Point	09040	Unit 1332 Heater SEP	2/1/2010	0.03	0.87
Point Breeze	non permit letter	Tk 33/35 Jump-over line	11/23/2010	0.03	0.00
Gir. Pt./Pt. Br.	RFD	3-Unit Train - Crude Transfer Pipeline	1/18/2013	Offset ⁵	0.00
Point Breeze	13001	Tank P-590 (PB 843) Reactivation ⁴	1/22/2013	Offset ⁵	Offset⁵
Gir. Pt./Pt. Br.	12270	Butane Truck Unloading at SRTF	3/5/2013	Offset ⁵	Offset⁵
Gir. Pt./Pt. Br.	13020	14-Unit Train - Crude Transfer Pipeline	4/8/2013	Offset ⁵	0.00
Point Breeze	RFD	210 Light-Ends Improvement Project	8/21/2013	0.01	0.00
Girard Point	RFD	Butane Logistics Project	1/13/2014	0.0005	0.00
Gir. Pt./Pt. Br.	12195	Heater Firing Rate Increase (7-Heater) ⁵	2/19/2014	Offset ⁵	Offset ⁵
Point Breeze	RFD	210 VTB Cooling	3/21/2014	0.002	0.00
Girard Point	14045	Butane Railcar Unloading	4/08/2014	2.70	0.56
Point Breeze	13260	South Yard South Flare	7/18/2014	2.42	1,44
Point Breeze	RFD	868 TCSS Distillate Recovery	6/9/2014	0.15	1.00
Girard Point	RFD	1232 Distillate Recovery	7/25/2014	0.30	2.08
Point Breeze	RFD	PB 210 V2 Stripper	7/25/2014	0.15	0.48
Girard Point	14219-14220	Butane Terminal Firewater Pumps	8/11/2014	0.00	0.00
Point Breeze	14237	Tank PB 36 (P-010) Gasoline Storage	8/29/2014	1.30	0.00
Gir. Pt./Pt. Br.	14149	Boiler 45	9/2/2014	1.45	5.06
Girard Point	RFD	1332 C-703 Steam Heat Exchanger	10/09/2014	0.01	0.21
Point Breeze	RFD	868 LCO Recovery Improvements	10/16/2014	0.11	0.75
Point Breeze	RFD	210C VTB Direct to 868	11/17/2014	0.03	0.21
Point Breeze	RFD	137 Depropanizer Feed	10/16/2014	0.00	0.00
Girard Point	RFD	433 Propane Processing Improvements	10/28/2014	0.16	1.00
Point Breeze	RFD	210 Debutanizer Cooling	Pending	0.00	0.00
Girard Point	RFD	1232 Absorber/ Stripper Tower	12/8/2014	0.00	0.00
Point Breeze	14368	Tank PB-848 Crude Storage	12/8/2014	1.01	0.00
Point Breeze	14369	Tank PB-844 Crude Storage	12/15/2014	1.01	0.00
Girard Point	RFD	GP 433 Emergency Relief	12/2/2014	0.00	0.00
Point Breeze	RFD	HDS Field Charge Pump	12/2/2014	0.00	0.06
Girard Point	RFD	Crude Off-loading Flexibility	1/8/2015	0.09	0.00
SRTF	RFD	Butane Blending at SRTF		0.00	0.00
Point Breeze	RFD	Tank PB-880 Crude Storage	3/2/2015 Pending	1.24	0.00
Point Breeze	RFD	Tank PB-880 Crude Storage Tank PB-850 Crude Storage	Pending	1.24	0.00
SRTF			Pending Pending	0.01	0.00
Point Breeze	Pending 14237	Butane Compressor		0.01	0.00
Point Breeze Point Breeze	Application	Tank PB 36 (P-010) Gasoline Storage Unit 864 PH-1, Unit 864 PH-11, Unit 864 PH-12	Pending Application	0.97	0.00
Tomic Diceze		Heater Burner Replacements	пррасинон		
	10-year	r increases/decreases from 1st Quarter 201 <u>5</u> 6		28.37	23.39

Notes:

- 1 The Effective Date of Change for emissions increases is considered the date of permit issuance and for emissions reductions it is the date of source shutdown.
- 2 Plan Approval 04237 triggered NSR for VOC.
- 3 Plan Approval 06144 triggered NSR for VOC & NOx.
- 4 Tank P-590 (PB 843) includes emissions from steam from No. 3 Boiler House that were already permitted in No. 3 Boiler House NO $_{\rm x}$ Reduction Project in 2008.
- 5 Plan Approval 12195 triggered NSR for VOC & NOx. All increases from calendar years 2009 through 9/6/13 (date of application) were offset.
- 6 Consent Decree emissions credits from the shutdown of the Marcus Hook 10-4 FCC and LSG units are not available except in certain situations as described in the Consent Decree.

Emissions Reduction Credits Available PES Refinery

^{*} PES is in active discussion with AMS regarding the accounting of emission reductions from the former Marcus Hook Refinery that were established while the facility was considered part of the Philadelphia Refining Complex. For the purposes of this application, these reductions are not considered contemporaneous.

1		_	_	_	_	_	_		
				Marcus Hook	Marcus Hook	Marcus Hook	Marcus Hook	. wearing	Facility
	1	Emissions credits nee		Consent Decree	Consent Decree	Consent Decree	Consent Decree		Parmit No
	Total Emissions Credits Remaining	Emissions credits needed in the 14149 Boiler 45 Plan Approval Application	Total Emissions Credits	Source 706 LSG Stabilizer Heater	Source 705 LSG HDS Heater	Source 040 10-4 Feed Heater	Source 101 10-4 FCC Unit	Course	Source
		plication		8/17/2012	8/17/2012	8/17/2012	8/17/2012	Directive Date	Effective Date
	-2.21		-2.21	-0.08	-0.13	-0.74	-1.26	VOC	
	-111.37		-111.37	-1.08	-5.14	-12.85	-92.38	NOx	Fourth Amendment to Consent Decree
	-128.42	• • • •	-128.42	-0.02	-0.01	-0.01	-128.38	SO_2	o Consent Decree - (
	-317.94		-317.94	-0.16	-0.29	-2.13	-315.36	PM ₁₀ PM ₂₅	Civil Action No. 05-0
	-365.6		-365.6	-0.31	-0.01	-0.36	-364.92	CO	2866 - Available Em
	-56.07	•••	-56.07	0	0	0	-56.07	H ₂ SO ₄	e - Civil Action No. 05-02866 - Available Emissions Credits, Tons
	-737,153.20	185,133.63	-922,286.83	-10,868.7	-16,551.0	-3,848.2	-894,018.9	CO ₂ e	-

Consent Decree Emissions Reductions can only be used for emissions units that meet the following criteria: 1 - For heaters and boilers, a limit of 0.020 lbs NO₂ per million BTU or less on a 3-hour rolling average basis.

- 2 For heaters and boilers, a limit of 162 ppmvd of hydrogen sulfide in fuel gas or 20 ppmvd SO2 corrected to 0% O2 both on a 3-hour rolling average, and 60 ppmv hydrogen sulfide in fuel gas on a 365-day average.
- 3 For heaters and boilers, no liquid or solid fuel firing authorization.
- 4 For FCCUs, a limit of 20 ppmvd NO₂ corrected to 0% O₂ or less on a 365-day rolling average basis; a limit of 25 ppmvd SO₂ corrected to 0% O₂ or less on a 365-day rolling average basis; and a limit of 0.5 pound of PM per 1000 pounds of coke burned on
- 5 For Flaring Devices, 162 ppmv hydrogen sulfide in gas burned in the flare on a 3-hour rolling average.

- 6 For Sulfur Recovery Plants, NSPS Subpart Ja emission limits.
 7 For emissions units other than those listed in items 1 through 6 above at which credits are being used, Best Available Control Technology ("BACT"), Best Available Technology ("BAT") or Lowest Achievable Emission Rate ("LAER"), as determined by

Attachment E
Best Available Technology NO_x Control Cost Effectiveness
Calculations

Tier 3 Project PES Refinery

BAT Control Cost Effectiveness Summary

	Α	В	С	D	н	F	G	Н	ı	J
Control Option	Potential Firing Current Rates Emission Rat (MMBtu/hr) (lb/MMBtu	Current Emission Rate (lb/MMBtu)	Potential Emissions (ΤΡΥ)	Control Efficiency (%)	Control Maximum Post Efficiency Control Emissions (%) (TPY)	Potential NO _x Reduced (TPY)	2013 Total Capital Cost (\$)	2013 O&M Cost (\$)	2013 Annualized Cost ¹ (\$)	2013 Cost Effectiveness (\$/Ton)
Unit 864 PH-7R Heater - SCR ¹	70.0	0.02	6.5	85%	1.0	5.5	3,153,207	109,882	757,414	137,461
Unit 870 H-3 Heater - SCR	110.0	0.03	14.5	85%	2.2	12.3	4,138,885	150,847	1,000,794	81,459
Calculation	on		= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

¹ SCR = Selective Catalytic Reduction

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mountain.		
Viimher of Years (n)	20	
interest Kate, % (1)	20	
Annualized Cost Factor (ACF)	0.21	

$$ACF = \frac{i(1+i)^n}{(1+i)^n - 1}$$

Cost Escalation Factor for Utilities ²	Cost Escalation Factor for SCR1	2013	1991	1986		Year	
1.57	1.78	567.3	361	318.4	Cost Index	Engineering	Chemical

¹ Cost data from Alternative Control Techniques Document - NO, Emissions from Process Heaters (Revised) - EPA-453/R-93-034 scaled from 1986 to 2012 costs using the

Cost Escalation Factor.

² Cost data from Alternative Control Techniques Document - NO₃. Emissions from Process Heaters (Revised) - EPA-453/R-93-034 scaled from 1991 to 2012 costs using the Cost Escalation Factor.

PES Refinery Tier 3 Project

Heater Capacity

Unit 864 PH-7R BAT Control Cost Effectiveness

Source Unit 864 PH-7R

Control SCR

Rated Heat Input 70.0 MMBtu/hr

Baseline Actual Emissions 6.5 Current Emission Rate 0.02

tpy lb/MMBtu

Control Efficiency 85%

10/1/11/1

GJ/hr

Evaluated at New Firing Limit at 2013 Cost and Efficiencies

73.9

Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034

_	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	3,061,366
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	3,061,366
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical;	
	piping; etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC)	3,061,366
INDIRECT INSTALLATI	ION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	91,841
TOTAL INDIRECT COS	TS, IC	91,841
TOTAL CAPITAL I	INVESTMENT (TCI)	3,153,207

PES Refinery

Tier 3 Project

Unit 864 PH-7R BAT Control Cost Effectiveness

Source

Unit 864 PH-'R

Control

SCR

Rated Heat Input

70.0

6.5

Baseline Actual Emissions

tpy

Current Emission Rate

0.02

lb/MMBtu

MMBtu/hr

Control Efficiency

85%

Heater Capacity

73.9

GJ/hr

COST COMI ONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	86,713 86,713
Utilities	
Ammonia Cc 4	941
Catalyst Repl wement Cost	22,227
Electricity Cc -1	0.1
Subtotal - Utilities	23,169
TOTAL ANNUAL DIRECT COSTS	109,882

COST COM ()NENT:	COST (\$)
TOTAL ANNUAL OGM COSTS	109,882
Annualized Cost Factor Equipment Life (years) = 20 Interest Rate (%) = 20 Annualized Cost Factor	0.21
CAPITAL RECOVERY COSTS TOTAL CAPITAL REQUIREMENT TOTAL ANNUAL CAPITAL REQUIREMENT	3,153,207 647,532
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized cap.t.1l cost)	757,414

PES Refinery Tier 3 Project

Unit 870 H-3 BAT Control Cost Effectiveness

Source Unit 870 H-3
Control SCR
Rated Heat Input 110.0
Baseline Actual Emissions 14.5
Current Emission Rate 0.03

MMBtu/hr

tpy lb/MMBtu

Control Efficiency 85%

GJ/hr

Heater Capacity 116.1

Evaluated at New Firing Limit at 2013 Cost and Efficiencies

Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	4,018,335
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	4,018,335
	Direct Installation Costs Foundations & supports; handling & erection; electrical;	
	piping; etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (1	TDC)	4,018,335
INDIRECT INSTALLATIO	N COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	120,550
TOTAL INDIRECT COSTS, IC		120,550
TOTAL CAPITAL IN	IVESTMENT (TCI)	4,138,885

PES Refinery

Tier 3 Project

Unit 870 H-3 BAT Control Cost Effectiveness

Source

Unit 870 H-3

Control

SCR

Rated Heat Input

110.0

14.5

tpy

Baseline Actual Emissions Current Emission Rate

0.03

lb/MMBtu

MMBtu/hr

Control Efficiency

85%

Heater Capacity

116.1

GJ/hr

COST COMI ONENT:	COST (\$)	
ANNUAL DIRECT COSTS	-	
Operation and Maintenance Labor		
Maintenance Labor and Material (2.75% of TCI)	113,819 113,819	
Utilities		
Ammonia Co-1	2,099	
Catalyst Replacement Cost	34,929	
Electricity Cc - I	0.2	
Subtotal - Utilities	37,027	
TOTAL ANNUAL DIRECT COSTS	150,847	

	COST (\$)	
TOTAL ANNUAL O&M COST	150,847	
Annualized Cost Factor	Equipment Life (years) = 20 Interest Rate (%) = 20 Annualized Cost Factor	0.21
CAPITAL RECOVERY COSTS	TOTAL CAPITAL REQUIREMENT TOTAL ANN UAL CAPITAL REQUIREMENT	4,138,885 849,947
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized cap. tal cost)		1,000,794

File Number: RECEIPT

AIR MANAGEMENT SERVICES

321 University Avenue Philadelphia, PA 19104-4543

Phone: (215) 685-7572 Fax: (215) 685-7593

15253

CITY OF PHILADELPHIA DEPARTMENT OF PUBLIC HEALTH PUBLIC HEALTH SERVICES

Location of Installation:

SUNOCO, INC. (R&M) **3144 PASSYUNK AVENUE** Philadelphia, PA 19145 Owner's/Contact's Name and Address:

SUNOCO, INC. (R&IVI) 3144 PASSYUNK AVE PHILADELPHIA, PA 19145

Philadelphia Code	Fund	Division	Dept.	Source	Fee
Minor Facility Permit	01	260	020	3201	\$
Indefinite License	01	260	020	3215	
Minor Facility License	01	260	020	3216	
Pennsylvania Code	Fund	Index Code		Source	Fee
Plan Approval	08	143582		3201	1700
Operating Permit	08	143582		3201	
Annual Administrative Fee	08	143582		3216	
Emission	08	143391		3216	

Air Management Services Contact: ED WIENER, CHIEF SOURCE RE

Date Received:

9/4/2015

VERIFY THE AUTHENTICITY OF THIS MULTI-TONE SECURITY DOCUMENT.

CHECK BACKGROUND AREA CHANGES COLOR GRADUALLY FROM TOP TO BOTTOM

PHILADELPHIA ENERGY SOLUTIONS REFINING AND MARKETING LLC 1735 MARKET STREET PHILADELPHIA, PA 19103



0001006609 August 29, 2015

64-1278/611 **VOID AFTER 120 DAYS**

¢x;x;x;x;x;x;x;**x**,**₹₹₹₹₹₹**

Amount: **One Thousand Seven Hundred dollars and 00 cents**

\$1,700.00

Pay to the order of CITY OF PHILADELPHIA 321 UNIVERSITY AVE PHILADELPHIA, PA 19104-4543

Bank of America N.A. Atlanta, Dekalb County, Georgia

Rachel Censeti AUTHORIZED SIGNATURE

VENDOR NO. 0000100226